NASA TECHNICAL MEMORANDUM

ASA TM X-62,412

(NASA-TM-X-62412) AN EXPERIMENTAL N75-21554
DOCUMENTATION OF A HYPERSONIC SHOCK-WAVE
TURBULENT BOUNDARY LAYER INTERACTION FLOW:
WITH AND WITHOUT SEPARATION (NASA) 67 p HC Unclas
\$4.25 CSCL 20D G3/34 18608

AN EXPERIMENTAL DOCUMENTATION OF A HYPERSONIC SHOCK-WAVE TURBULENT BOUNDARY LAYER INTERACTION FLOW — WITH AND WITHOUT SEPARATION

M. I. Kussoy and C. C. Horstman

Ames Research Center Moffett Field, Calif. 94035



 		O District Control Ma
1. Report No. NASA TMX 62,412	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle		5. Report Date
AN EXPERIMENTAL DOCUMENT	NTATION OF A HYPERSONI	
SHOCK-WAVE TURBULENT BO	OUNDARY LAYER INTERACT	
FLOW - WITH AND WITHOU	Γ SEPARATION	
7. Author(s)		8. Performing Organization Report No.
		A-5910
M. I. Kussoy and C. C.		10. Work Unit No.
Performing Organization Name and Addr	186	506-26-22-00-21
Ames Research Center		11. Contract or Grant No.
Moffett Field, Calif.	94035	
		13. Type of Report and Period Covered
2. Sponsoring Agency Name and Address		Technical Memorandum
National Aeronautics a	nd Space Administratio	n 14. Sponsoring Agency Code
Washington, D. C. 2054		
6. Abstract ,		
presented for two shoot flows, respectively. shear and heat-flux di interaction regions. boundary-layer profile were obtained from which were derived. The data	k strengths resulting The surface measurement stributions upstream, At closely spaced intensions of static and pitot ch velocity, density as are presented in both citient detail to valid	in attached and separated its include continuous pressure, in, and downstream of the ervals along the surface, pressure and total temperature and static temperature profiles the graphical and tabular form. date advanced computer codes
17. Key Words (Suggested by Author(s))	18. Dist	tribution Statement
Boundary layer	Un	classified - Unlimited
	1	27A
	İ	STAR Category - 34
	20. Security Classif. (of this pe	21. No of Pages 22 Price*
19. Security Classif. (of this report)		67 \$4.25
Unclassified	Unclassified	J

AN EXPERIMENTAL DOCUMENTATION OF A HYPERSONIC SHOCK-WAVE TURBULENT BOUNDARY LAYER INTERACTION FLOW — WITH AND WITHOUT SEPARATION

M. I. Kussoy and C. C. Horstman

Ames Research Center

SUMMARY

An experiment, thoroughly documenting the flow field resulting from the interaction of a shock wave with a nonadiabatic hypersonic turbulent boundary layer, is described. Detailed mean flow and surface data are presented for two shock strengths resulting in attached and separated flows, respectively. The surface measurements include continuous pressure, shear and heat-flux distributions upstream, in, and downstream of the interaction regions. At closely spaced intervals along the surface, boundary-layer profiles of static and pitot pressure and total temperature were obtained from which velocity, density and static temperature profiles were derived. The data are presented in both graphical and tabular form. These data are of sufficient detail to validate advanced computer codes and their associated turbulence models.

INTRODUCTION

As a result of the recent rapid advance in computational fluid dynamics, it is now possible to obtain solutions to complex flow fields using the time averaged Navier-Stokes equations. However, the pacing item for successful solutions to strongly coupled viscous-inviscid turbulent flows is turbulence modeling. To validate or develop new turbulence models one must rely on thoroughly documentated experimental flow fields. To provide sufficient experimental detail for validating computer codes or turbulence models, the minimum requirements for an experiment must include surface measurements of pressure, shear and heat flux as well as mean flow profiles. Fluctuating measurements are necessary if higher order turbulence model closure schemes are to be evaluated. For high-speed compressible flow the zero pressure gradient case has been experimentally examined in great detail. However, for flows with pressure gradient or separation there are only a few examples of documented flow fields (refs. 1, 2, and 3). Until more experimental flows are documented over a wide range of test conditions, the development of generalized turbulence models for flows with severe viscous-inviscid interactions will remain unresolved.

This paper presents experimental data for two shock-wave turbulent boundary-layer interaction flows, one with separation and one without. The measurements include surface pressure, shear and heat flux, and detailed

profiles of pitot and static pressure and total temperature throughout the interaction region. The data should provide the detailed information necessary to validate many of the new computer codes and turbulence models currently being developed.

SYMBOLS

М	Mach number
p	pressure
P	static pressure
P INF	local free-stream static pressure ahead of interaction
q	heat flux
r	radial coordinate, distance from model centerline
RHO	density
RHO INF	local free-stream density ahead of interaction
RHOU	mass flux (pu)
RHOU INF	local free-stream mass flux ahead of interaction
T	temperature
T INF	local free-stream static temperature ahead of interaction
TT	stagnation temperature
TT INF	local free-stream total temperature ahead of interaction
u, U	velocity component in axial direction
U INF	local free-stream velocity ahead of interaction
x	axial coordinate, distance from leading edge of shock-wave generator
y, Y	distance normal to model surface
α	wedge angle of shock-wave generator
5	boundary-rayer thickness

ô* compressible displacement thickness,

$$\int_0^\delta \left(1 - \frac{\rho u}{\rho_e u_e}\right) \frac{r}{r_w} dy$$

 $\delta_{\mathbf{i}}^{\star}$ kinematic displacement thickness,

$$\int_0^\delta \left(1 - \frac{u}{u_e}\right) \frac{r}{r_w} dy$$

 θ compressible momentum thickness,

$$\int_0^\delta \frac{\rho u}{\rho_e u_e} \left(1 - \frac{u}{u_e} \right) \frac{r}{r_w} \, dy$$

 $\theta_{\mathbf{i}}$ kinematic momentum thickness,

$$\int_0^\delta \frac{u}{u_e} \left(1 - \frac{u}{u_e} \right) \frac{r}{r_w} dy$$

ρ density

τ shear stress

SUBSCRIPTS

c corrected

e edge of boundary layer

i initial value

m measured

o stagnation conditions

T wind-tunnel stagnation conditions

w wall

local free-stream ahead of interaction

DESCRIPTION OF EXPERIMENT

Facility

The experiment was conducted in the Ames 3.5-Foot Hypersonic Wind Tunnel where heated high-pressure air flows through a 1.067-m diameter test section to low pressure spheres. The nominal free-stream test conditions were: total temperature = 695° K, total pressure = 34 atm, free-stream unit Reynolds number = $10.9 \times 10^{\circ}$ m⁻¹, free-stream Mach number = 7.2. The test core diameter was approximately 0.7 m with an axial Mach number gradient less than 0.12 m⁻¹. Useful test time was 3 min. Run to run variations in pressure and Mach number were less than 0.5 percent. However, the wind tunnel total temperature varied up to 50° K from run to run and also during a single run it varied about 50° K over the 3 min test time. These variations required special data reduction procedures which will be discussed later. Free-stream fluctuation measurements, reported in reference 4, have been made in this facility at the above nominal test conditions. The average total temperature and mass-flow fluctuations were 0.83 and 2.7 percent, respectively.

Mode1

The test model consisted of a cone-ogive cylinder, 3.3 m long and 0.203 m in diameter and an annular shock-wave generator, 0.51 m outside diameter, mounted concentric with the cylinder (fig. 1). The entire model was water-cooled maintaining a constant surface temperature at 300° ±5° K during a run. Interchangeable instrumentation ports, 12 cm in diameter and specially contoured to fit flush with the cylindrical surface, were located at 25 cm intervals along the cylinder in a single line and every 50 cm in another single line 180° away. Individual ports were instrumented with static pressure taps, thermocouples, or a skin friction balance. One port accommodated a survey mechanism to which static and total pressure and total temperature probes could be attached for flow field surveys. Additional static pressure taps and thermocouples were located every 5 cm along the entire model length in a single line 90° away from the instrumentation ports. At several stations static pressure taps were located every 90° around the model.

Two shock wave strengths were imposed by beveling the leading edge of the generator at either 7.5° or 15° resulting in unseparated and separated turbulent boundary layers, respectively. The details of the two generators we shown in figure 1. The leading edge of each generator was hone! sharp before each test. The generator was movable in a direction parallel to the axis of the cylinder so that the entire interaction region could be passed over selected sure y station.

Instrumentation

Confine Pressure. The model static pressure taps, located along the model surface as well as in several instrumentation ports, were 0.16 cm $^{\circ}$

inside diameter connected with short lengths of stainless steel tubing (10 to 15 cm long) to strain gauge absolute-pressure transducers. The transducers were calibrated prior to the test series with a dead weight tester and several in situ calibrations were made before selected runs by varying the wind-tunnel test section pressure using a manometer follower as a standard. All calibrations were linear and repeatable to within 1 percent. Prior to each run a transducer reading was obtained at the wind tunnel starting pressure (approx. 0.01 atm) to determine the zero offset of the gauges. All the transducers were located within the model and water cooled.

Surface Heat Transfer .- Surface heat transfer was measured by the transient thin-skin technique. Five instrumentation ports, using the same material and thickness (1.25 cm) as the model to avoid any temperature discontinuities along the model surface, were instrumented with chromelalumel thermocouples spot welded to the interior surface. The thermocouples were spaced 2.5 cm apart in a line parallel to the model axis. One port, 0.625 cm thick, was also instrumented with thermocouples spaced 1.25 cm apart. Depending on the thermocouple location, the temperature rise (with the internal model water cooling disconnected) varied from 10° to 50° K during a typical 30-sec heat-transfer run. The data were reduced by obtaining a least squares linear fit of $\ln \left[(T_T - T_w)/(T_T - T_{wi}) \right]$ versus time. The variation of the wind-tunnel total temperature (T_T) with time was included. No discernible differences in the measured heat transfer were obtained by using the two different thickness ports. Calculations using the procedures outlined by reference 5 indicated for the present test conditions, the interior wall temperature follows the exterior wall temperature after 2 sec and that longitudinal conduction errors are less than 5 percent of the measured convective heat transfer. Therefore no corrections were applied to the data.

Kistler floating element skin friction balance. The sensitive portion of the gauge was 0.95 cm in diameter by 0.05 cm thick. The entire gauge was contoured to match the radius of the cylinder. Direct calibrations using weights hung from the sensing element were performed before and after each test series; they were repeatable and in agreement with the factory calibration to within 5 percent. In addition the gauge was equipped with a self-calibrate coil, providing an electrical calibration before and after each run. These calibrations were also within 5 percent of the factory calibration, and an average of the two electrical calibrations were used to reduce the data for each run. Since the floating element was relatively large, a buoyancy correction was necessary to account for the forces across the gauge element due to the longitudinal pressure gradients.

Survey Mesianier. Flow field surveys were obtained with the survey matchanism sketched in figure 1. A precision nower screw was driven by a stepping motor, whose shaft was capable of turning in controlled increments as small as 1.8° or any multiple of 1.8°. The vertical resolution of this mechanism is 0.0003 cm. The rotary motion of the motor shaft is coupled to the precision screw with antibacklash bevel gears and the vertical position was obtained from a three-turn precision potentiometer driven by an antibacklash worn gear.

by stainless steel probes shown in figure 3. The larger probe was used at each survey station. Near the wall, a smaller probe (half size) was also used. The second probe (fig. 3), with the tip much closer to the supporting strut, was used in the separated region to ensure that both the probe and its strut were within the separated region. This probe was also used facing both upstream and downstream in the separated region. The probes were calibrated in a free-jet facility-matching Mach number, velocity and density with the present test conditions. These calibrations indicated that the errors due to rarefaction effects were less than I percent; therefore, no corrections were applied to the pitot data. These probes were attached to water-cooled pressure transducers located within the model with short lengths (5 to 10 cm) of stainless steel tubing. The pressure transducer calibration procedure was identical to the surface pressure procedure discussed previously.

measured by stainless steel probes shown in figure 4. The larger probe was used at each survey station while the smaller probe was used in the separated region facing both upstream and downstream similar to the pitot probe measurements. These probes are geometrically similar to those used in reference 6, i.e., a 10° cone-cylinder. Independent calibrations to account for viscous interaction effects agreed with the calibration of Bearens (ref. 6). The maximum viscous corrections applied to the data were 2 percent in and downstream of the interaction regions and 7 percent in the undisturbed region ahead of the incident shock wave. These probes were attached to water-cooled pressure transducers located within the model with short lengths (5 to 10 cm) of stainless steel tubing. The pressure transducer calibration procedure was identical to the surface pressure procedure discussed previously.

Total Temperature Probes.— Total temperatures in the flow field were measured with the probes shown in figure 5. The larger probe was used at each survey station while the smaller probe was used in the separated region. These probes were designed using a concept suggested by Vas (ref. 7). An unshielded, butt-welded chromed alumel thermocouple (0.3 cm long by 0.007 cm thick) is supported by tapered chromel and alumel posts. A second chromelalumel thermocouple is formed at the end of the alumel support (see fig. 5). This provides a simultaneous measurement of the butt welded thermocouple junction and the probe support.

Corrections for radiation, conduction and recovery factor were made following the method of reference 7. To make these corrections the local Mach number and Revnolds number must be known, thus, requiring an iterative procedure using the pitot and static pressure data. For the present cases, radiation corrections were negligible. Independent calibrations of these probes in the wind tunnel free stream indicated a maximum total temperature error of 1.5 percent.

Test Procedure. The test data were obtained during a series of runs with the wind tunnel operating at the nominal conditions described above. Previous measurements (ref. 8), without the generator, established the

existence of a fully developed, self-similar turbulent boundary with negligible pressure gradient 100 to 300 cm from the model tip. Natural transition from laminar to turbulent flow occurred between 40 and 80 cm from the model tip.

For the surface pressure and shear measurements the shock-wave generator was moved axially during a run to obtain continuous data along the model. To accomplish this, the generator was held in a large frame which moved axially either upstream or downstream. See figure 6. Its speed was controlled by a variable speed motor and its position recorded by a potentiometer attached to the frame. The total travel was 25 cm varying from 140 to 165 cm from the model tip (see fig. 1). During a run the generator was occasionally stopped to insure that the measurements were not affected by instrumentation time lags. For the surface heat transfer and flow-field surveys the generator was prepositioned at a fixed axial position prior to a run. At all times the shock-wave generator was located several cm behind the intersection of the bow shock emanating from the model tip and the annular plane of the generator. For the separated flow case several pitot and static pressure runs were also made keeping the probes at fixed distances from the wall and moving the generator.

The undisturbed boundary-layer thickness at the incident shock-wave impingement point increased about 10 percent in a distance corresponding to the difference between the farthest upstream and downstream positioning of the shock-wave generator. However, this had little effect on the experimental results (including the flow field surveys) provided they were compared an equivalent distance from the generator leading edge.

Velocity, density, and pressure profiles were obtained from pitot and static pressure and total temperature surveys. Each survey was taken during a single test run. In traversing the flow field, the probe was stopped at each location for a few seconds to ensure no time lag in the pressure or temperature measurement. Survey data were obtained up to 3.5 cm from the model surface except at the initial survey stations where data were obtained up to 8 cm. The static pressure at the model surface was monitored continuously during all traverses to verify that the data were free from interference effects.

Axisymmetry.— Surface pressure measurements at selected axial positions were obtained at 90° intervals around the model and serface shear measurements at selected axial positions 180° apart. Variations in these data around the model were within the experimental accuracy of the measurements. Also, results from surface all film studies showed symmetric separation and reattachment lines around the model for the separated case and a symmetric incident shock line for the attached case. From all these results it was concluded that a flow was axisymmetric.

EXPERIMENTAL RESULTS

Local Free-Stream Conditions

Surveys of pitot and static pressure and total temperature were obtained at several axial locations upstream of the interaction region for both cases to determine the local free-stream conditions ahead of the incident shock. Above the boundary layer the variation of the measurements with distance from the model surface (up to 8 cm) was negligible. The average local free-stream values are tabulated in tables 1 and 2 for the two test flows. Slight differences are noted between the two cases which are believed to be caused by small differences in wind-tunnel blockage.

Flow-Field Features

Sketches of the two flow fields constructed from survey data and shadow-graphs taken during the experiment are presented in figures 7 and 8. Several features of the flow fields are worth mentioning. Unlike most two-dimensional experiments that employ long wedge-shaped generators, the present flows are influenced by an expansion fan generated by the corner of the shock-wave generator. Both flows indicate an induced shock wave caused by a lifting of the boundary layer although the strength of this shock wave is significantly less for the attached case (α = 7.5°) and eventually coalesces with the recompression shock far downstream. For the separated case (α = 15°) the location of the induced shock wave was unsteady due to the unsteady nature of the unseparated flow. The unsteady aspects of this flow will be discussed later.

Surface Measurements

Variations in surface pressure, shear and heat transfer with distances from the leading edge of the shock generator are shown in figures 9 and 10 and tabulated in tables 3 and 4 for both test flows. These data are average values obtained from many runs. Scatter bars indicating the maximum data scatter from run-to-run are shown for several locations along the cylinder. In tables 3 and 4 both the measured and corrected (for longitudinal pressure gradient) values of the surface shear are presented. In figures 9 and 10 the corrected values are plotted. The surface heat-transfer data were not corrected for the small longitudinal conduction errors (less than 5 percent) but were corrected for run-to-run variations in wind-tunnel total temperature. This was done by assuming that the neat flux divided by the driving potential $(T_{\rm Ti}-T_{\rm Wi})$ is invariant for small changes in total temperature. Therefore;

$$q_{corrected} = q_{measured} [(T_{T_i} - T_{w_i})_{nominal}/(T_{T_i} - T_{w_i})_{measured}]$$

The surface measurements for both the attached and separated flow cases show the major features associated with a shock-wave boundary-layer interaction; a steep increase of pressure (with an intermediate plateau for the

separated case); a decrease in skin friction (leading to negative values for the separated case) followed by a rapid increase; and a corresponding increase in heat flux. An exception from the usual two-dimensional experimental results for this type of flow is the rapid decrease in pressure, shear and heat flux downstream of the peak values which is a result of the expansion fan emanating from the corner formed by the leading edge and the body of the shock generator.

Separation and Reattachment

One of the more difficult aspects of the experiment was precise determination of separation and reattachment point locations and of values for skin friction in the neighborhood of these points. One reason for this was the unsteadiness of the separated region. The unsteady features were examined with a new diagnostic technique that measured the fluctuating voltage from thin platinum films deposited on the outer surface of one of the instrumentation ports. Results for the present flow have been reported previously (ref. 9). Briefly, those results showed that separation and reattachment points experienced large excursions, indicating a maximum separation zone from x = 28 to 39 cm. The frequency of the unsteadiness was confined to a narrow band around 15 kHz. Assuming a convection velocity equivalent to the average boundary-layer velocity ahead of separation, the scale of the unsteady motion was estimated to be approximately equal to the length of the separation as determined from the skin-friction measurements which showed separation at x = 31.5 cm and reattachment at x = 34.0 cm. (Direct skin friction measurements, not corrected for buoyancy effects, show this same extent of separation.) The separation appears to be similar to that found in incompressible flow (ref. 10) wherein onset and reattachment locations are intermittent and only when the flow is reversed 50 percent of the time or more will time-averaged measurements like pitot pressure and skin friction indicate separated flow. Additional data defining the length of separation were obtained from forward and backward facing pitot probes. These data, obtained at fixed values of y and varying x by moving the shock generator, indicate a slightly larger separated region than the skin-friction measurements extending from x = 30.5 to 34.5 cm. The authors feel that the best estimates of the time-averaged separation points are given by the pitot probe technique. Furthermore, the accuracy of the skin-friction data in the vicinity of these points is uncertain due to the unknown influence of unsteadiness on the floating element balance. No satisfactory explanation has been found for the odd behavior in the skin-friction data just ahead of separation.

Flow Field Measurements

Velocity, density, and pressure profiles normal to the cylinder surface were obtained from pitot and static pressure and total temperature surveys. In most cases, more than one survey of each type measurement was obtained at each data station. The data presented were obtained from average values of the measured pressure and temperature interpolated at selected y locations. The run-to-run variations were less than 5 percent. To account for

the run-to-run variation in wind tunnel total temperature, the measured values of total temperature were corrected assuming that the ratio $(T_0-T_W)/(T_{0_{\mbox{e}}}-T_W)$ was invariant. Therefore,

$$T_{o_{corrected}} = (T_{o_{e}} - T_{w})_{nominal} \left[\frac{(T_{o} - T_{w})}{(T_{o_{e}} - T_{w})} \right]_{measured} + T_{w}$$

The flow quantities, Mach number, velocity, static temperature, and density, were calculated assuming a calorically imperfect, thermally perfect gas.

Normalized profiles of static pressure, velocity, and density are presented in figure; 11 and 12 for the attached (α = 7.5°) and separated (α = 15°) flow cases, respectively. These data along with additional flow-field quantities are tabulated in tables 5 and 6. To illustrate the details of the interaction regions, the profile data have been used to construct static pressure, velocity, and density contours and are shown in figures 13 and 14. The locations of the incident, induced and recompression shock waves are easily recognized. Further details of the interaction regions are shown in figures 15 and 16 where streamline contours, deduced from the velocity and density profiles, are given.

The integrated values of incompressible and compressible displacement and momentum thicknesses, δ_i^\star , δ^\star and θ_i and θ_i are given for the two cases in tables 7 and 8. Also included is the boundary-layer thickness, δ_i^\star , used for the upper limit of integration. The choice of a boundary-layer thickness for these types of interaction flows is rather arbitrary. For the present case, δ_i^\star was chosen as the height at which the pitot pressure was a maximum in the interaction region; and downstream, where the pitot pressure continuously increased, δ_i^\star was chosen where the local Mach number profile no longer had curvature and varied linearly with distance from the wall.

Experimental Uncertainties

The uncertainties in the surface pressure, shear and heat flux measurements were estimated to be ±10 percent except for the shear measurements near separation for the separated case and near the minimum shear value for the attached case. Here, because of the large buoyancy corrections, the uncertainty is extremely high (up to 50 percent of the upstream undisturbed value). In addition, the unsteady aspects of the turbulent separation may cause additional unknown errors in the skin-friction balance measurements near separation. For the flow-field quantities, the estimated uncertainties are 11.5 percent for the total temperature, 10 percent for the static pressure, :6 percent for the static temperature, :12 percent for the density, and ±3 percent for the velocity. For the separated case near the wall (v < 1.0 cm) in the interaction region (x = 30 to 36 cm), the uncertainty in velocity is ±8 percent; in the reversed flow region, it is +35 percent. The uncertainty in y is 0.02 cm. However, these uncertainties in the flowfield variables are due principally to zero offsets in the pressure measurements. Since each survey was obtained with a single probe, the uncertainty of the vertical variation in these flow-field quantities is significantly less than the numbers quoted above.

CONCLUDING REMARKS

Two cases of a shock-wave, hypersonic turbulent-boundary-layer, interaction flow over a cone-ogive-cylinder were experimentally investigated. For one case the boundary layer was attached and in the other the shock wave was of sufficient strength to separate the boundary layer. The mean flow field measurements of surface pressure, shear and heat flux, pitot and static pressure and total temperature profiles were completely documented. The tabulated results presented in this report provide, in sufficient detail, experimental data for validating present or future computer codes and/or turbulence models.

REFERENCES

- 1. Sturek, W. B.: An Experimental Investigation of the Supersonic Turbulent Boundary Layer in a Moderate Adverse Pressure Gradient. Part 1. A Detailed Description of the Experiment and Data Tabulation. BRL Report No. 1506, Oct. 1970.
- 2. Voisinet, R. L. P.; Lee, R. E.; and Yanta, W. J.: An Experimental Study of the Compressible Turbulent Boundary Layer with an Adverse Pressure Gradient. Paper No. 9, Turbulent Shear Flows, AGARD-CP-93, London, V. K., Sept. 1971.
- 3. Rose, W. C.: The Behavior of a Compressible Turbulent Boundary Layer in a Shock-Wave-Induced Adverse Pressure Gradient. NASA TN D-7092, March 1973.
- 4. George, A. R.; and Reinecke, W. G.: Conduction in Thin-Skinned Heat Transfer and Recovery Temperature Models, AIAA Journal, Vol. 1, No. 8, Aug. 1963, pp. 1956-1958.
- 5. Owen, F. K.; Horstman, C. C.; Stainback, P. C.; and Wagner, R. D.: Comparison of Transition and Freestream Disturbance Measurements Obtained in Two Wind Tunnel Facilities, AIAA Paper No. 74-131, Jan. 1974.
- 5. Behrens, W.: Viscous Interaction Effects on a Static Pressure Probe at M = 6, AIAA Journal, Vol. 1, No. 12. Dec. 1963, pp. 2864-2866.
- 7. Vas, I. E.: Flow Field Measurements Using a Total Temperature Probe at Hypersonic Speeds, AIAA Journal, Vol. 10, No. 3, March 1972, pp. 317-323.
- 8. Horstman, C. C.; and Owen, F. K.: Turbulent Properties of a Compressible Boundary Layer, AIAA Journal, Vol. 10, No. 11, Nov. 1972, pp. 1418-1424.

- 9. Horstman, C. C.; and Owen, F. K.: New Diagnostic Technique for the Study of Turbulent Boundary-Layer Separation, AIAA Journal, Vol. 12, No. 10, Oct. 1974, pp. 1436-1438.
- 10. Sandborn, V. A.; and Liu, C. Y.: On Turbulent Boundary-Layer Separation, Journal of Fluid Mechanics, Vol. 32, May 1968, pp. 293-304.

TABLE 1
7.5° SHOCK WAVE GENERATOR

$M_{\infty} = 6.71$	$\rho_{\infty} = 0.0300 \text{ kg/m}^3$
$P_{\infty} = 607 \text{ N/m}^2$	$U_{\infty} = 1129 \text{ m/s}$
$T_{\infty} = 70.6^{\circ} \text{ K}$	$T_{O_{\infty}} = 695^{\circ} K$
$T_{W} = 300^{\circ} K$	

TABLE 2

15° SHOCK WAVE GENERATOR

$M_{\infty} = 6.86$	$\rho_{\infty} = 0.0312 \text{ kg/m}^3$
$P_{\infty} = 607 \text{ N/m}^2$	$U_{\infty} = 1132 \text{ m/s}$
$T_{\infty} = 67.8^{\circ} \text{ K}$	T _{O∞} = 695° K
$T_W = 300^{\circ} K$	

TABLE 3 7.5 DEGREE SHOCK WAVE GENERATOR

w _b o _{w1} w _m y _d x	(N/m^{-}) (N/m^{2})	3860. 71.8	3740. 71.6 67.6	3640. /1.1 6/.1	2540. 70.6 A6.7	3450. 70.1 66.3	3360. 69.6 65.9	3280. 69.0 65.3	3190. 68.4 64.7	3100. 67.7 64.1	3030. 67.1 63.6	2980. 66.3 63.0	2900. 65.7 52.4	2830. 64.8 K1.6	2760. 64.1 60.9	2700. 63.4 60.2	2410. 61.8 58.7	2490. 59.6 56.9	2410. 58.1 56.3	2210. 56.4 53.7	2210. 54.4 52.0	2100. 52.5 50.1	2030. 50.5 48.2	1940. 48.8 46.7	1900. 47.6 45.5	1910. 45.8 43.8	1720.	. 660	• 0000		1390.	1330	1270.	1250.		1210.	1140.	1167.	1130.	1100.		
ō*																									31200											•				·	37300	
	, E																																							72.6 48.6		
-	.																·				• C r C r	• •	• C C C C C C C C C C C C C C C C C C C	•																• O C E 77 C		
*	:	, i	, <mark>.</mark>	٠,٠	,	,	· ·	. 4	0	ur u	· ·			٠,	a	• "	• ′	• 6	• C	• • (•		• (. 4 . r	•	ب	,		•	•	9.6	,	•		• • 3	•		• }	• ;	• (• •	

TABLE 4 15 DEGREE SHOCK WAVE GENERATOR

,, ,	,3	مخنو	*	£	أنو	j	œ
	, () 	4,	•	3	£	ن بخ	* مخبو
	(E / Z	(-E/*)	(cm)	(N/m)	(N/m+)	(N/m²)	(M/M)
	7.6.7	6240.	42.0	5690	78.9	82.2	54600
		6240• 6240•	7 0	.0274	7 ° °	9,78	54500
	16.7	6360.	2 t 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5680.	0 00 0 00 0 00 0 00 0 00 0 00 0 00 0 0		54100
	16.7	6580.	0 • 44	5620.	88	7 48	53700
	16.3	6810.	¥ • 77	5540.	89.7	85.3	53200
	17.4	7040.	6.44	5450	70.7	P.5.4	52707
	17.4	7260.	7 * 7 7	55.00	91.7	85.1	52200
	G	760".	0 • 9 7	£240.	92.2	86.3	5150C
	14.3	7940.	44.K	<130°	7.20	96.5	50905
	1.06	8400.	0.44	5010°	92.2	95.8	50200
	11.6	.0806	47.5	4890°	¢1.9	95,3	49500
	7.5	9550.	0 0 0 7	7470	7.15	7.74	48800
	18.1	10200.	¥ • a †>	4450	20.0	83.9	47900
	و. ج	11000.	0.00	*0237	00.00	4 ° c a	47200
	a •	11900.	u • 0 *	4430	5.0a	62.7	46300
	17.2	12900.	© • C v	.300.	£ 9 d d,	0.1.0	45400
	R • 2	1440C.	ਖ • ਹੁਬ	4190.	87.3	80.9	4450C
	4.7	15906.	C • [V	4070	RF.1	0.01	43600
	1.4	1770/	د] • د	3966.	84.8	78.7	4260
•	α. •	21000.	J • 6 5	3 B 5 0 •	83.6	7-7-	4170.
•	7.5	24400.	¥ ° C U	3740.	B. 2 . 4	76.7	4070
•	رد د د	28100.	ر. • د ب	3640.	° 08	75.4	39706.
	٥.	31200.	५ • € ७	3640	70.4	74.1	3880C.
	α α	34300.	C • 24	34E0.	77.8	72.7	3790°
	α	37500.	¥*73	3340.	16.0	71.0	37060.
	27.5	3 9 900 •	() • y y	3250.	74.5	49.7	36100.
	14.3	42700.	មិ-មិម	1160.	72.1	۴۵,	35200.
	10,7	45100.	66.0	3000°	71.1	64.5	34300
	4.6.1	47230.	3 · 4 2	3000°	69.1	44.7	33500
	5.7.	49100.	57.0	2910.	67.2	0.63	32700.
	, a,	\$7880£	67.6	2 R 3 O.	67	61.6	3180
	644.7	5220°	C • α ν	2760.	63.	a • 0 4	3096
	3. E. A.	• 23300	ਪ • ਹ ਪ	2690.	62.3	η. Α.	30100
	ų • c.	£4000	C • 0 ¥	26.25	40.A	£7.3	29300
	۲. ،	2440	u • C u	16 A.O.	٠٥.	α • u u	28500
	ţ.	544000	J • U9	2480.	57.0	64.3	27830
	عر <u>۽</u> ج	\$470C.	¥0,4°	,010°	6.4°	y • ₹ 'y	27100
			0.14	234.0	4, 6, 6	5,2	364.00

TABLE 4 — CONCLUDED
15 DEGREE SHOCK WAVE GENERATOR

o, 3	(W/m²)	ď	520	094	410	350	290	250	9	100	010	930	960	190	730	570	500	550	510	0.9	0.2	370	330	0 8 0	07	90	50	00	090	020	~	"	_	90	~	Š	8740.	Ę,	$\vec{-}$
μ, 3.	(N/m^2)	51.2	50.4	49.5	48.6	47.8	6.97	46.0	45.1	F 3 . 7	£ 0 47	41.2	39.6	38.5	37.4	36.2	35.3	34.3	13.7	33.0	32.0	11.1	10.7	30.0	58.4	2 A . A	28.3	27.8	27.4	27.0	26.5	26.0	25.5	25.0	24.5	74.1	93.9	73.7	23.6
, RE	(N/M^2)	54.4	53.4	52.5	51.5	50.5	46.5	48.5	47.6	46.1	44.3	0.64	41.2	40.2	38.9	37.8	36.8	35.8	35.1	34.3	73.3	32.6	71.9	11.1	30.4	29.7	29.1	28.4	27.9	27.5	27.0	26.5	24.0	25.5	25.0	24.5	24.3	1.42	24.0
7	(N/m ²)	2	21	7	80	5	ç	91	•	7	Ş	7	S.	4	7	38	32	26	21	٧.	Ξ	ع	č	•	~	-	O	10	~	_	\sim	0.0				~	717.	_	~
×	(cm)	_	<.	⋄	~	٠,		,t	v.	٠	٠.	α•	•	ċ		٠.	ė	-7		Š	•		•	٠,	•	•		:	٠				•	٠.	•	•	C • E C	•	•

ORIGINAL PAGE IS OF POOR QUALITY

TABLE 5 7.5 DEGREE SHOCK WAVE GENERATOR

~	.S DEGRE	E SHCCK	MANE GENE	IFRATCR.	X = 42	MO 0.		7	.5 CEGREE	F SHCCK	HAVE GEN	GENERATOR,	77 H X	1 0	
(,)) A	ĸ.	, a a	PEC INF	TINE) U ()	RHOL / RHCU INF	11 / 11 INF	¥ (C#)	1	P /	RHO / RHC INF	1 / T	U INF	RHCU / RHCU INF	11 / 11 INF
0000	00000	ာ ့	•	. 25	0	220.2	0.432	202-2	000.0	1.000	0.235	.25	8	သ	0.432
0 v 0 v 0 v	1.027	000.1	C - 204	4.856	0.330	2.094	0.632	0.050	90.4	000	0.208	4.841	0.353	0.088	0.607
्र • • • • • • • • • • • • • • • • • • •	1.655	00		: ;		0.117	0.694	001.0	1.620	1.000	0.222	.51	5	1-	669.0
3 - 1 2 5	1.917	00.	•	.22	.5	0.135	0.744	3.125	116.1	000-1	0.236	• 24	. 58	.13	0.744
0.1150	? , 7 • ?	ر. د	•	- 1.	•	251.	0.773	0.150	2.C84	1.000	C.245	• 08	•62	• 1 5	6.173
175	2.167	0	•	55.	ç.	0.162	C. 784	0.175	2.184	200°.	0.252	3.964	45.	91:	C. 784
· ·	2-2-3	0	•	98.	•	0.170	0.794	C - 200	2.30C	200° I	C.263	္ ရွ	9	~ [`	651.0
2 4 7	2.348	0 0	•) 9 1 ° 0	0.80	0.250	2.411	300.1	0.271	\$ 0,0	6.5	E 0	708.0
) •	20 4 02	၁ ် •	•	. 4	•	0 W	10.0	2000	7 . 4 . 5	000-1	0.00	0			0.874
) J	7				`~	0.201	C.830	004.0	2.671	0000	0.295	38	. 7.3	7	0.830
) () () ()	7.9€?			4.	•	0.269	0.836	0.450	2.752	1.000	0.304	.29	. 74	.22	0.836
0000	119.5	00.	•	.43	•	C+215	0.842	0.500	2.831	1.000	C.312	.2C	. 75	• 23	0.842
	2.ele	00.	•	• 26	•	5.235	C-852	0.600	2.908	1.000	C.318	. 1 4	. 16	.24	0.852
0.730	805.5))	•	-	•	0.243	C.864	0.10C	3.C28	000-1	0.331	.02	. 78	• 25	0.864
32 P • 3	1.055	00•	•	€ 05	•	C-262	0.873	0.800	3.128	1.000	0.341	.93	• 19	.27	0.873
(6.)	3.212	1.000	•	• d¢	٠	6.283	286.0	იი6*ე	3.333	1.0CC	C.367	.72	₩.	30	298.0
ر. در ا	3.346	ر ر	•	7	٠	308.0	0.892	1.000	3.463	200.1	C. 384	•60	30	.32	0.892
1.150	47 4.5	000	•	.62	•	C+32C	0.901	1.103	3.563	1-coc	0.395	53	8	. 33	106.0
1 - 202	3.6.17	٠, د	•	. t.	•	0.344	0.9cg	1.200	3.657	1.000	0.413	24.	•	.35	606-0
1.40%	3.755	<u>ر</u> َ	•	3.5	•	C.362	C.917	1.300	3.815	1.000	624.0		₽,	.37	0.917
			•	2.363	•) • 38C	(200	30 5.	795.5) () () ()	7 4 4 4 C	77.	3 0 4		5 0 0 0 0 0 0 0 0
, pe • • •	4.00) - -	•	201.7	•	3 F 6 7	0.00	000	611.4		C * * C	7 7	• •	7.4	25.0
, () • ·	1.703	;	•		•	77.0	440	200.1	244		004	9 0	. 9		0.00
000	()	,, ∈ , . •	•		• •	~ - -	6 6 9	008-1	049.4	000	0.559	0	` '	. 5.	0.953
0 0	2 · · · · ·	. ر . ر	• ,	. ~		0.46.0	0.00	1.900	556.4	1.000	28.5	1.709		. 54	0.960
	7. 5. 4	1.000		1.620		6.583	(.967	2,000	6.023	1.000	0.626	• 55		. 59	C-957
2010	6.143	33.	•	.54	•	C. E15	(16.)	2.100	5.146	1.000	657.0	1.518	ů,	.62	0.573
3.50	5.11.	ر. دن	•	*	•	0.666	0.973	2.200	5,363	1.000	0.691	1.448	٠.	• 66	0.979
77	5.50m	Ç	•	• 3¢	•	504.0	0.965	2.30c	£.	1.000	C-124	19.1	o.	. 1C	0.985
30 ₹* €	. 163	•	•	5.7	•	٠, ۲	C 6 3	604-5	109.5	220-1	0.756	1.323	٠,	. 7.5	0.990
	5.580	3	•	. 2.	•	8 C	*c 5 * 0	. ୨ ଏଠ	3 4 6	1.ccc	6.8.3	1.531	ς.	~	765.0
	£ - 1 74	ပ္	•	-	•	e.	C 5 6 3	2.600	0.(44	1.000	C.834	1.200	J.	.82	0.997
2.700	4.234	۲,	•	17	•	π. π.	0.49P	2.100	€-238	1.000	C • 8 8 O	1.136	٠.	à.	8.0°0
0.4.		0.	•	٠ د د	•	5	2.900	2.800	6.343	1.000	506°0	1.10	٠.	36.	666.0
⊃ C & • €•	1.000	C.	•	€0.	•	96.	1.000	3.900	6.481	1.000	246-3	Ç	٥.	.53	1.000
	5.0.0	ر • د ر	•	^-	•	. 5.7	1.000	000.	5.5.9	1.000	6.507		٥.	35.	1.033
) (T.	240.0	00.	•	⊃ ∵•	•	9	1.000	3.100	4.616	1.000	6.615	• 05	٥.	٠٤٧	1.000
302.4	t. + 6 5 5	1.000	•	\mathbf{a}	•	99	1.300	3.200	6.115	1.000	1.032	955.0	0	ွင့	1.000
3.300	4.702	100.1	•	٠ د ن	٠	. 5.5	1.000	3.300	6.140	1.511	1.524	٠ و	3	55	1.001
77	6.728	1.000	•	ė,	•	20.	0000-1	304.6	6.157	2.45	2.447	36•	?	4.8	1.000
3.500	¢.722	1•000	•	<u>ټ</u> ح	•	္	1.000	3.500	6.1 07	110.	2.548	÷.	Ç.	. 52	

TABLE 5 7.5 DEGREE SHOCK WAVE GENERATOR

		7.5 DEGREE	E SHOCK	MAVE GEN	FRATCR.	95 H	#3 0°			1.5 CEGREE	E SHOCK	HAVE GEN	GENERATOR,	¥ ×	#0 C#	
	¥ (C4)	1	/ 6	KTC /	1 / 1) 	N DOHA	11 / 11 !NF	¥ (C#)	1) d	AHO INE	TINE	c INF	RHOU /	11 / NI TI
0				<u>-</u> ر	-		2									
RJ	0.300	000°	1.023	O	5		220-2	₹.	0.000	000.0	2	0.294	4.252	80	ö	Ĉ,
G	0.0.0	156.3	1.023	0.208	\$06°5	C-328	6.068	0.597	0.050	591	36	C-212	6.43C	6.223		0.727
N	5.0.0	1.205	1. (23	0	4 '		60.0	۰	2.0	219.0	7 P	0.220	6.729	35	5.5	7
'Δ'	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	155-1	1.023	ۍ د	~ -		0.10	•	0.125	7.7.7	· W	C-227	6.766	5	ô	76
m	P 4) ~ - 0	1001	<i>)</i> (- 0		7710	``	0.150	C . 8 5 3	· U	0.238	6.681	*	G	78
T) h	0.00	7001) ()	9		C•153	٦.	C. 175	6.917		0.243	6.732	35	S	
		y	1.023)	2		0.159	_	C.20C	0.576	•	1,500	690.0	3	ဌ	80
_	7	7 2 2 4 7	1.023	, ()	۳		0.175		0.250	1.221	1.048	6.265	6.201	£ .	۲,	0.814
_	0000	2.346	1.023	U	33		C.183	۳,	0.300	1.402	1.636	C-219	5.856	8,	7	30.0
	0.350	2.417	1.023	Ç	2		261.3	æ	0.350	1.600	1.614	0.296	5.44.7	Ų.	9 -	, a
	0.04.0	₹° €	1.023	ر.	5.7		551.0	Ψ.	C.43C	1.693	1.586	662-0	2.7.6	7		. 4
	C 4 * * .	2.50	1.023	,	Š		0.205	œ,	0.450		1.034	116.0	2000	ē 3	7	4
	0.500	2.65r	1.623	Ç	0		6.217	₾.	005.0	555°1	1.000	176.0		. 3	3 7	
	(00.1	2.136	1.623	ر،	æ		C.227		704.0	407-7	1 T T T T		1062	5 6	, ,	8
	0.700	. F 74	1.023	٠ ر	?		0.244	.			1.466	70.00			. 5	8
1	• • •	1200	1.623	,	9		C. 763			2.631	1,330	*****	3.211	~	5	.87
-	٠.	10.4	, , , , , , , , , , , , , , , , , , ,) (J 1		2000	•		3.136	1.295	0.435	2.919	8	5	.89
	000-1	377.6		۰, ر	ם ט		0 · C · C	o ca	1.100	3-322	1.239	C.442	2.800	8	36	
) (715		, .	· 0		1 CL		1.200	3.635	1.170	0.407	2.505	8	ž	9.
		r a	110	, ,	, ,		4 4 6 C		1.300	3.865	1.125	0.484	2.326	9	*	93
) (. 4 		=======================================	, _			C.374		1.400	4.049	1.080	0.4.0	2.237	ě	4	
		,) 10) U	110-1	, (,	. ~		404.0	· ·	1.500	4.144	1.057	0.498	2.167	5	1	96
	/ () ()	47 - 4		, . ,			0.425	٠,	1.600	4.218	1.045	C-485	2.153	6	4	96.
	~ ·	4.3.15	000		-		0.460	٠,	1.700	4.311	1.034	0.492	2.103	Ġ.		9.0
	000	1, 7	1.011	ر. ا	39		0.493	0.949	1.800	4.389	1.057	C • 513	2.059	9	ž (
		4.479	1.01	ر	7.7		0.530	0.955	1.900	4.55.9	8 7 1 .	265.0	2 6 5 5 T	2 0	, 4	3 6
	500.5	4.876	1.011	0	<u>ئ</u>		6.55	0.960	2.000		11	7.0	0 4 7			000
		ور دري دري		-, (a.		40.4°C	\$ 100 c	001.7	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2.420	1.725	1.403	٠.	. 3	1.000
	, , ,	7.0	(٠, د	~ ~		7 6	. 64.0	2.100	5.659	2.670	1.578	1.350	85.	6	Ű
) " 4 • 4 • 10		1.00.	, .			C. 736	C • 982	2.43€	5.729	2.566	2.244	1.322	٧.	~	1.000
	004	4 6 6			32		0.116	250.0	2.500	411.5	3.051	2.370	1.364	9.58	m	80
	004.0		7.7		=		0.832	0.965	2.600	5.800	3.102	2.397	1.294	85	•	80
))	6 B 6 5	1 - 4 7 7		2		1.125	1.000	2.730	5.780	3.136	50402	1.302	φ.	Ĕ.	ġ (
	1	 	100°		. ~ . ~		2.173	1.000	2.830	5.805	3-136	2.427	1.297	96	~ ;	္တ ု
		\$ 7 A B	. 36.		5		2.467	1.000	2,960	5.863	3.125	7.417	1.293	96.	,	3 :
	, 50° F	5.77	d		5		2.501	1.600	000.€	5.8c1	3.114	• 4 C	1.293	φ	Ť.	30
		1	1.175	•	-		2.562	1.000	3.100	5.ec7	3.102	3	1.251	ر م	Ť,	30
	, ,		9 3 t . t		~		2.491	1.000	3.200	5.863	3.CBB	2.373	5 6 7	or c	•	3 3
		7.0	3.420	•	1.350		2.483	1.000	3.300	5.783	990.	£ ;] · · · ·	<u>ت</u>	~ ~	300
	1.4.5	5.641	3.46	Ī	4		2.460	1.000	3.400	5.765	200 · C	2 . 34 7	1.30.	7 9	· `) C
	1.590	. 5 5 6	3.436	•	3.7		2.437	1.000	3.500	447 00	3.637	٠,	1.310	Ď	7.	3

ORIGINAL PAGE IS OF POOR QUALITY.

TABLE 5

TABLE 5

7.5 DEGREE SHOCK WAVE GENERATOR

•	.5 [.f.GP	FF SHCCX	BAVE GENER	FRATOR.	X = 54.	W) 0,	-	7	.5 CEGREE	E SHCCK	DAVE GENE	NERATOR.	X = 56.	X 0.	
•	•	,						3	1	4		1	`	RHOU /	/ 11
¥ (₩)	•	\ <u>\</u> a a	PHC INF	1 / T) 	RHCC INF	- 1 1 N L	ر	1	P INF	AHC INF	T INF	∴ INI		- Z
		•			(_	4	00000	0,000	7.818	_	4.252	0.000	0.000	0.432
100.0		43.0	_	4.25			r -		1.259	7.818	~	6.015	654.0	6.557	0.801
0.0.0		6.54	<u>.</u> ; .	6.25	714.0	_	200	0.00	1.333	1.813	_	5.433	0.483	0.636	0.813
440.0		6.50				•	608-0	001.0	1.371	7.618	_	4.654	0.498	C.654	178.0
10 T - 1		F . 5	<u>.</u>	11:		•		6.125	1,355	1.795	_	5.965	C. 507	C-662	0.836
3.124		£ . 4		7 .	r r r · · ·	•	α α α	7 1 5 (1.425	7.784	_	2.960	0.518	0.676	0.840
C. 15.		£ . 37	-	5.12		•	2 4 2 4 2 6	175	1.455	7.173	_	5.939	C.527	0.69°	0.852
		f. 34	-	,	C (C (C (C (C (C (C (C (C (C (•	, G	0.200	1.4.90	7,761		5.919	0.536	0-102	C. 858
				70.0			2 4	3.250	1.555	7.739	_	5.812	0.558	0.743	2 8 6 7
152.		6.29	_		110.0	•	7.85.	00100	1.636	7.765		5.687	0.581	C-787	0.879
0		6.2	-		(, 55 t		(A		1.718	7.659		5.560	09.0	0.831	0.890
		6.2.	-	5.59	384.J		7 6 6	004	0. C.	7.614		5.287	0.636	0.91e	0.89
7,7		6.21	-	7.5	1 1 1		, o		100.2	7.545		120.5	879.3	1.004	0.00 C
					7 P				2 - 1 4 2	1.400		4.779	0.698	1.096	0.920
704.5		9.16	-	,			7.0.0	0000	2.486	7.273		4.196	0.759	1.316	0.0
36		<u>ب</u>	-	*	0.00		440	000	2.922	7.034		3.551	0.821	1.626	3.964
3.735		Ź.,		ا م	(400	006	2.276	6.841		3.144	0.866	1.884	0.990
		4	a4	~	n (1000		3.819	6,614		2.539	C. 907	2.363	556.
		<u>ن</u>		7 · C			000	000	546.4	6.364		150.2	C.937	2.853	1.000
		•	٠	- '	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \				4-713	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1.837	0.952	3.152	000°1
3 · ·		0	~+	-			200	207	510.5	5.523		1.656	£96.0	3.211	1.000
1.23.		* .	۲,	٠,)		000	202.1	72	4.886		1.575	6.968	3.001	1.000
ç 		•	~	-	* * * * * * * * * * * * * * * * * * *		000	004-	5.200	4.091		1.500	6.56 8	2.539	200.
1.40.		ပ် က	~	Ξ.	n - 0		000-1	1.500	5.232	3.500		1.544	696.7	751.2	700.
1.50		7.1	•				000		5.341	3.235		1.491	0.972	2.111	
1.600		3.2	114		ביים מיים מיים		200	1,700	804.5	3.205		1.46C	0.974	2.13ë	000-1
1.700			٠,	-	1		000.1	008-1	£.3HB	3.318		1.4669	0.974	551.2	000°1
30F.		•	٠,	* •	- C		000	1.99	04.6	3.500		1.492	215.0	2.201	1.000
1.600		*	^.	₹ • ·	700		000	2000	157.5	3.693		1.513	0.671	2.371	700.
			~ (0 m		000.1	2.100	5.284	3.867		1.518	C. 671	2.454	
-		•	,		(C		1.000	7.200	5.310	3.864		1.504	7.0	264.7	000
767.7			,		185.0		1.000	2.336	5.310	3.864		0 . 0 .	2.0	2010	000
•				7.1	0.985		000·1	2.400	0 7 6 6	7,63,6		7 D 7 0 1		653.2	1.000
•			•	1.0	4 X 7 . 7		1.000	2000	0.50	50000		1 4 8 3	0.07	1.932	1.000
•				1 • 2	* 25 to - 0		eeo•1	000	7	2 705		1.457		1.865	1.000
			•	1.2	0.58 *		0.00.1	20102	# U * U			1.450	5	1.850	೦೦ ೦ ₹
· 7			Ī		1.96.0) (O O O	0.00	937 4	2.761		1.462	5	1.84C	1•000
,		3.	•	-	6.7 3.		000.		5 . 4 . A	27.0		1.451	6.1	1.839	1.000
		~	•	-	2 8 5 ° C		2000	000.	427	2.139		1.451	6	1.834	1.000
71.		~			20°0			007.7	5.412	2.139		1.458	5,	2.8.1)00 *!
000	4.7.4	4 + + · ·		2.20			2000		5.408	2.121	1.865	4	476.0	1.820	1.00.
·		· .		<u>.</u> -	ی د ان ۲		000.1	3.400	55E*\$	2.121		1.404	5	* C C C	700
**		,			. e.	: :	1.000	3.500	5.379	2.121		r ~	5	100.1	· · ·
7. 40 40						•		_							

1 1

ORIGINAL PAGE IS OF POOR QUALITY

TABLE 5
7.5 DEGREE SHOCK WAVE GENERATOR

"	.s eture	FF SHCCK	BAVE GE	NERATCR,	8 ×	¥. 0.			7.5 CEGRI	EF SHCCK	NAVE GENE	IERATOR,	09 * ×	. C C	
1 * 0) k	ı	P INF	PHC /	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	N IN	PHCU /	11 / 11 1NF	4 (CM)	1	P / q	RHC /	1 / T	U / U INF	RHCU /	71 17
000.0	3.000	9.023	1.847	4.252	00000	200.0	0.432	00000	ು	7.500	1.704	4.252	00000	9	643
	1.213	507.	50 K • •	1.143	1441	C.582	0.864	0.050	2	7.386	1.228	6.015	694.0	ייי	0.804
	7	7.766	1	- Co	0.486 0.486	0.653	0.815	5.015	1.496	7.352	1.314	5-593	0.527	C.652	0.818
	() () () () () () () () () ()		706-1	7 4 8 4 6		5.65.0	0.830 0.030	ે. ડે. !	٠,	7.330	1.327	5.522	0.552	۲.	0.835
	1000	3000	P (P)	26105	これのよう	C • 743	0.841	0.125	٠.	7.27?	1.328	5.477	6.566	۲.	0.844
	1 . 4 .	C W W A	7.5.4	1.00	2 u	*	0.847	0.150	91	7.216	1.330	5.426	0.579	~	0.852
	1	7 8 2	7 4		() () () () () () () () () ()	95/-0	248.0	521.0	~ '	7.159	1.311	5.377	0.589	^	0.858
	1.645	7.0.7	5. 7 -	4 4 4 4	7	0 0 0 0	C.852	J. 20C	٠.	7.102	1.326	5.354	C.597	-	0.864
	7.40	7 20 0 0	7 4	1 FC - C	1 A C • 3)	C 8 C	2.250	αņ,	7.645	1.343	5-245	0.619	æ	0.875
	2 2	7.00.4)	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0)) () () ()	ŗ.,	C . 080	800	5.108	0.641	بده	0.886
	1.446	7.523	1 - 4 7 4			\$ 10 mm	1 to 0	2001	. د	5 5 5 5	504.1	E 60 1	663	o,	3.894
	2.082	7.39H	1.520	1.00.1	400	(*) • —	100.0	0 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- ^	C 9 4	764-1	4.13.7	2. 688 0	Ġ,	0.905
	2.213	1.164	1.595	4.044	C. 711	1.127	0.623	0000	•	7.41	1 547	*****	C	. ب	516.0
	2.578	7.17C	1.77c	4.037	3-77	1.171	0.043	0000	•	100	107.1	4.01.3	0.1.00	٠,	0.923
	8 * 5 * 5	7.114	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1.513	40.00	4 4 4	140	00.	9 0	20.0	10.7	* · · · · · · · · · · · · · · · · · · ·	* (8)	N.	156.0
	3.348	160.	256.3	3-627	T 40 T	0 4 0 7 - (~ د	70.0	747	47.50	0.824	c ·	0.953
	4.7.5	7.646	762	1	. 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 7 7 7	000		٠,	****	761.7	4 6 4 5 5	0.865	œ.	0:6.0
	44.744	3 4 4 7	2 7 4			7		0 0		101	#1C * 7	7 6 6 7	T	7	C. 980
		t. 103	. Z.	910-1	4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	7 1 4 1 7		200	ų ū	5 F T V	2.683	841.7	165.0	اند	466.0
	156.0	6.477	1000	1.785	0.55	1000	000	1.200	, ,	5 C V C	3 - 1 - 1) * * * * * * * * * * * * * * * * * * *		,	1.000
	4.004	5.966	06.	1.562	698.0	3,46	1.000	1.300	- 00	0.00	3.238	1.860	664.0	ۍ ز	000-1
	1.01.	5.364	1.437	1.561	C.96P	3.328	00001	000	ō	2075	1.165	704		õ	000.
	9	122.4	7 E.O. 4	1.531	J15.7	455.6	1.030	068.1	دَن	5.114	3.131	1.633	100.0	٠.	000
	7) 85. ;	964.7	1.487	0.473	2.341	000.1	1.630	-4	4.716	3.015	1.564	0.00	ΰ	200-1
		3.091	2.132	1-450	3.976	2.078	1.000	1.700	~	4.148	2.680	90	0000	ď	
	* ·	9.66.0	7,0*7	1.412	115.0	5.004	1.000	1.80c	2	3.523	2.269	1.553	696.0	Š	2000
	\$ ^		\$ 6 .7 (7 E 7	546.0	1.005	1.00·1	1.900	•	2.858	2.052	1.412	C. 577	್ರ	1.000
		ָ ב ב ב	3	1.476	£ 6 5 0	2.023	200.1	5.000	-	2.67C	2.022	1.321	0.582	~	1.000
		1) c	161.7	1	~ ~ · · · · · · · · · · · · · · · · · ·	2.(74	000.1	2.100	ď	2.500	1.460	1.275	C. 585	9	000-1
	C 3 C * .	36.5	3 4 7 6 7			2-150	000-1	2.705	Š.	2.50€	1.874	1.334	6.581	1.835	1.000
-		46.	7 J	*75.1	\	7.181	1.091		4 (2.50c	1.732	1.443	6.975	1.685	1.000
-	سر ، ز د ، و ،	C. T.	7.4.7	0 44 - 1	24.0	2 3 8 6		200.0	V (2-500	1.6.4	i.520	0.971	1.596	000.1
	,		111	7 5 7	7 6 0	2000) () (, t	376.5	1.675	1.644	C.964	1.565	1.000
			404	7	980	, ,) [/	7 6 6	7.00.7	D	26.65	1.663	1.78€	0.956	1.586	.300
	1	70.	7 0	D	() 7 • 0	6.51	000	ت ت ا	=	3.409	1.130	2.005	(.543	1.662	000-1
-	; ,		5 4 4 7 - 4 7	- C		5.56.5) ·	256.7	- :	3.523	1.704	2.C&8	0.939	1.599	000.1
Ī	· ·	4 1. F.			0 	: or :	1.00.	002.7	_ :	1.523	1.704	2.068	0.939	1.544	000.1
٠	, , ,				· ·	200	200. 200.	٥ ٥ ٠	•	\$ \$ \$ \$ \$ \$ \$	1.644	2.C24	0.541	1.586	,00°.1
•				* * * * * * * * * * * * * * * * * * * *	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1.764	1.000	3.100	4 (3.125	1.658	1.885	C.95J	1.574	1.030
•		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	, ,	, ,	2 · · · ·	۲۲.))	1.20(2.841	1.632	1.741	C. 45A	1.563	000.1
٠	· :	7 7	4 1 6 7	7.74.1		a	300·1	3.300	- 1	2.841	1.632	1.741	6.958	1.563	220.1
•) ~ • !		E .	# ·	70.0	12/1) () () ()	30 4.	~ 1	7.841	1.632	1 - 7 - 1	0.958	1.563	0000
		つつ!!!!	1.1.	174.1	4/6.3	1.71	1.000	3.500	~	2.841	7:9:1	1.741	C.558	1.563	000
							-								

TABLE 5 7.5 DEGREE SHOCK WAVE GENERATOR

	7.5 CEGRI	EF SHOCK	.S DEGREE SMOCK HAVE GENERATOR	EPATOR,	× + 62			,	.S CEGRFF	F SHOCK	NAVE GENE	ERATOR,	ж 49	1 000	
S D D	£	4 / d	RHC / RHC INF	1 / 1 INF) n	RHOU /	TT / TT INF	Y (CM)	τ	jųl d	RHC INF	1 / T	U U N	RHOU /	11 / 11 INF
300° b	3.	0.765	~	~	ဝ	00000	•		00	00	4	. 25		220-2	0.432
550 Q	1.329	6.682	1.120	ě.	C. 483	0.541	0.815	0.00	1.785	5.535	1.157	5.127	600	69	
C		r.e.30	-	1	3	0.156			9	36	2	19	0	۶2.	•
o Q		6.59	-	-	9	192.3			٠٤٥	8	£.	.77	65	80	•
35.53	1.6	6.58C	1.2	.15	4,)	0.783			S	8 .	53	7	9 .	<u>ي</u> د	٠
12 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		6.545	1.2	90.	6.2	508.0	•		ဗိုင်	e i	23	71.	9 4	20	
	Ŧ.	6.523		9	9	0.813 0.013			֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		, ר	֓֞֝֝֓֞֜֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֜֓֓֡֓֡֓֡֓֓֡֓֡֓		9	
25/20 04/4/	(200.		m () () () () ()	0 4	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•		7	۲,	- 2	4.4	` ~	5	
	· ~	7 00 4	-	8 6	9	450.0			2	5.5	m	.25	~	15.	
265.75	•	541.4		4	7	0.083			43	61	۲,	.2c	۲.	Ď.	•
		, , , , , , , , , , , , , , , , , , ,		~	73	1.030			56	58	e.	55	. 7		•
		\$ \$ \$ \$ \$ \$ \$ \$	-	.:.	7.5	1.104			69	53	5	98.	₽;	<u>.</u>	•
354.3	2	5.852	7	<u>ن</u> • ون	8	1.300	•		<u>ن</u> ج	3.5	Š.	٠ د د د د	0	7.4	•
2,736	7.	5.852	-	5 !	6	1.534	•		- :	٠. د	- 9	2 6	0 4		
5(e*0	**	5.618	· , ,	ar i	£ 9	10,01	•		. ~	, 4	<u></u>		. 60	8	, ,
		5.64.		E (6	2 2 2 2				3.5	, m	34	3		•
700	,	0 6 6 3	, , ,	٠, c.	. 0	2,662			56	28	5.	.05	6	7.	•
	•	70134) a	ď	2.918			9	27	. 76	96.	4.	£2	•
202 · 1				. 7.2	5	3.0.6	•		.82	.27	5	. 17	55	ž.	•
	•	4.466		m	\$	3.127	•		55	.21	Ξ	.69	ŷ.	56.	•
		5.341		·	6	3.122	•		90	25.	$\frac{1}{2}$	69.	5	ب ت	•
J. 6. I	ur.	3.17C		_	Š	3.087	•		-:	_;	7:	30.	9.	ა - მ	•
1.700	· ·	4 - 5 4 3	*	•	8	2.999	•			ָרָ עַ		, r	, 3	ָב פ כ	• •
008-1		4.765	· .	1.584	o i	2.8.2	•		-	נינ			ָר ני	5 0	
900°1	•	117.6	` `	1.376	, 0	7.617	•		, ~		9 05	1.570	25	06	
170°	,	. 143	-	404.	7	078.1	0			31	9	. 48	2.	.82	
71 · 7		4-0-		1.387	6	1.847	00		. 50	. 7	÷¢.	7.	6	39	
201 · 1		7.456	-	1.345	ò	1.790	2		ė.	99	7	1.554	?	5	
(* · · ·	Ţ	5000		1.34C	3	1.681	00.		<u>ن</u>	س ر	æ,	1.254		80 4	
ý • ·		1.265		Š	-	1.546	0.		,	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	- (1 7 7 - 1	r 0	ָ ע	
004.6		2.132	-	1.276	G (1.496	1.000 1.000		ي ر		č) a		2 4	
, (,	,	160.		3 ·	جَ وَ	784-1	9		ب د	- 4	,	1.277		•	
JC 8 • .		* 0	<u>.</u>	1.359	7 0	1001	9 9			7 (J	•	2.7	Š	1.350	
િ. •	,		: .	7 0		7.5				α.		~	Š	3	
) ! ! !	;				Ü	5.5			· ·	48	1	80	35.	7	
		0 m	-		Ü	1.526	00		-	4	3	٤2.	5	5	000-1
1) (1) (1) (1) (1) (1) (1) (1) (1) (1) (,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-		,	1.522	3		-	23.	ŭ,	. 2 t	C	3	1.000
, C Y) W () W	: _	7.00	س.	1.499	0			4.	3,	125.5	٠	4	1.000
(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	•	600	: :	E 75	ċ	1.490	3		.26	36.	4	٠.	0	-	1.000
>>· • 6	•	: •					_	_							

TABLE 5

	7.5 CEGRE	E SHCCR	MANE GEN	ERATOR.	ж 9	¥.0 0.		1	.5 CEGPE	E SHOCK	MAVE GEN	NERATOR,	8 8	#3 0°	
(W) A	¥	٠, ١	7 0 1 2	1 / 7) 	AHCU /	11 / INT	Y (CM)	Ł	4 4	AHC INF	1 / T) J J	RHOU /	17 / 11 1NF
		-				•				•	•				
7000	ن	5.39B		25		0.000	0.432	000°0	0.000	96	1.154	4.252	00000	220.2	0.432
0.000	-	5.398		36		0.554	0.818		1.641	96	1.010	3 0	•	119.0	80
6.015		5.358	-	-		0.711	0.832		2.144	98	1.128	<u>ښ</u>	•	0.751	2
001.0	?	5.358	-	4,0		0.816	0.846		2-282	89	1.180	∹'	•	18.0	5
0.125	~	5.35P	-	7		C-823	0.855		2.328	£.	1.189	Ç		C.835	Ď,
0.150	~	5. 358		4.5		0.82C	0.864		2.347	٤٦.	1.189	∹ '	•	C-842	80.0
₹ (1 ° ° °	~	5.386		-		0.848 0.0	C-870		2.404	.86	1.201	ر,	•	C.868	9
0.50	~	5.341		34		0.856	0.878		5 - 4 4 5	, E¢	1.22.1	5	•	C.888	an i
057.0		+37.		6.3		0.893	D. P. B. C.		5.509	e.	1.236	٥.		C. 516	20,0
	~	5.227		71.		C-923	0.855		2.543	. e.	1.242	æ		576-0	8
	~	5.148		99		C.958	0.903		2.596	. 8.4	1.262	æ		C*85.7	8
() () () () () ()	~	5.068	-	8,		665.0	6.939		2.696	.83	1.305	•		500.1	· ·
	-	685.4		64.		1.041	416.0		2.156	63	1.355	•	•	1.067	5
	· ~	ر س چ		5		1.112	0.920	3.500	2.867	€3	1.396	4		1.106	3
00000	, ~·	* BBC		2.4		1.233	0.932	3.630	3.082	.63	1.500	2	•	1.237	6.0
202-1	~	9.26.	_;	55		1.362	0.943	C. 10C	3.269	. E3	1.603		•	1.356	46.
		7 7		7.		1.573	0.955	008-0	3.455	9.	1.701	æ		1.473	0.980
,	~	A 2 2		. 4.		1.760	0.966	⊃8 6• 0	3.68C	. 76	1.825	٠.	•	1.617	96
, -		4 6 6 3 6		17		1.536	0.977	000.1	3.938	19.	1.959	۲,		1.776	6
	•	E 1 9 5 7		(C)		7.156	0.984	1.100	4-164	69	5 0 0 9 9	?		1.537	0.588
		4. AC 7		2		2.362	2.647	1.200	196.4	5.5	452.2	਼	•	2.109	60.
		4 - 76 1	~	7		2.583	೦೦೧ - 1	1.330	4.584	.62	2.416	5		2.284	0.996
(u	4.739	113	47.	υ,	2.180	1.000	1.400	4.807	. 62	2.603			2.487	66.
		4.127	~	53	J	2.891	1.000	1.500	256.4	.62	2.768	•		2.663	00
	ar.	4.71e	~	4	6.564	2.556	1.000	1.600	5.070	¢ 5	2.840	1.628	•	2.739	1.000
001-1		4.659	~	٠٤١	٣.	5.984	1.360	1.706	5.14C	~	5.899	•		2.803	1.000
	J.	4.014	~	.50	٠.	2.985	1.030	008.1	5.177	٠,	2.935	•		2.840	300.1
1.90	•	4.544	~.	4.	٠.	2.95€	1.000	006•1	5.186	9.	2.536	v.	•	2.842	300-1
700-1	•	4.25.	~	¥ .	7	326.2	1.000	2.000	612.5	£.	2.924	•		70 G	
2013	ų,	4.330	~•	. * .	۳.	398.2	1.000	2.100	5.245	4.	2.903	٠,	•	C18.7) (O) (O) (O) (O) (O) (O) (O) (O) (O) (O
2.200	•	40704	٧	٠,	σ,	2.823	ာ (၁၂)	2.230	5.272	9				751 - 7	000
20.13	4	16).4	,	Ţ	٠.	2.781	000·1	2.300	5.214	4. 4 4. 4	148.7	•	•		000
(64.	•	408.4	٠,	<u>د</u>	·-	2.120	20C • 1	2.400	3 P P P P P P P P P P P P P P P P P P P	()	6.86.3	116.1	•	2 716) ()) ()
	ď	3.625	~	•	Σ.	1.0.7	2000	200.	2.26.1	,	00° 00° 00° 00° 00° 00° 00° 00° 00° 00°	•		044	
2000	u	4.66	- 1	Ç.	ς.	518 - 2	າດດ.:	ာ (၆)	5,535	ه د	7 . 7 . 7	**************************************	•	2.63.5	
`.' √	¥°			2∼.	•	700))) (7000	2000	֓֞֜֜֜֜֜֜֓֓֓֓֜֜֜֓֓֓֓֜֜֜֓֓֓֓֓֜֡֓֓֓֡֓֜֓֓֡֓֡֓֡֓֡֡֡֡֡֓֡֓֡֡֡֡֡֡	20107		•	795 6	900
1. 1.	•	5-623	_	. 23	٠,	1.614	0.0.1) (a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	11	\$ ^ \$0 .	163.7	, y - 1	•	7 511	
605.7	۷.	1.564		7	•	/ / * -	00001	006.7	7.03	Ç,	# - C - V	, ,	•	7 7 7	
	•	1.70		,		505°	56.0•1	000.5	100.0	* (0.2.	D - C	•	404	
	Ð	7.440		<i>y</i>	•	1.365	700	3.100	236.6		740-1	., ,	•	,	
, (, ,	v	4 ·		٠ ا 4	•	1.322	1.07	3.200	5.719	σο U	ລດຊ•1		•	7/ **1	000
. 36 .	4.35.3	٠, ٢٠٠	_	. 61-1	665.0	1.316	्ट्ट ः ।	3.300	6.798	1.761	1.360	1.295	•	D 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	000
004.	٠.	3.0.5		en U	<45°	1.323	000-1	3.400	5.863	40	¥05.4	٠,	•	10276	222.
3, 4.	•	3.056		٠ ان	0,45.0	1.360		3.500	5.923		****	•	•	217.1	000-4
							_								

TABLE 5

GENERATOR
WAVE
SHOCK
DEGREE
7.5

	7.5 CEGREE	EE SHECK	MAVE GEN	GENERATOR,	x = 70.			,~	7.5 DEGRE	F SHOCK	V	GENERATOR,	x = 74.	ပ္	
Î	X.	P (NF	RHC (NF	1 / 1 [NF	o o in	RHOU / RHOU [NF	17 / 17 [NF	YCMI	I	P / P INF	RHG /	T INF	U 1NF	RHCU /	TT / TT [NF
9 (0,1	4.4.3	1.045	25	00.0	90.	2.0	000.0	9	9	C 895	\$5.	00	ö	4
ر ا ا	2.233	4 . 4 . 4 . 4 . 4 . 4 . 4 . 4 . 4 . 4 .	1.057	4.202	C.682	0.721	C.847	0.000	2.328	3.867	1.624	3.717	0.091	2.0 2.6 8.5 8.5	0.764
00	*.	4.643	•	• 54	C.712	8c	•85	0.100	*	9.	•06	• 56	69.	ř	w
ر د : د	*.	4.443	•	96	6.719	ခ်ိန္	• 86	5.125	5	96	60.	.55	7.	٠,	œ,
. v	• •	* * * * * * * * * * * * * * * * * * *		7.0	527.5	9 -6	 	0.175	Ň	ກ 60	1.066	51	7.	~~	
0	٠.	4.432		25.	C.137	. 63	98	0.200	4	9.	20.	5.	, 2	, .	700
٠,	٠,	4.432	•	.80	0.754	.88	.89	0.250	~	٠,79	.00	.48	. 75	8	œ.
	÷	4.43.3	•	. 74	C. 76.3	05.	90	0.300	~	. 78			-1	80	ری
ु <u>र</u>	٠.	4.432	•	.62	د. 178 م	25,0	2.0	0.350 	ě,	6	1,125	4.	4.0	60,0	م م
2 (- 3	25.5.5	•	. 4	0 0	0.0	76		0	-	- 5	7	. 6	- 6	
2000	حي د •	4.426	٠.		C. 809	140-1	92	3.530	Š	7	, ; ;		, w	5	` '
9	Ξ.	4.420	•	57.	C.826	4	.93	209.2	5		25	96.	.83	6	٥,
20	?•	4.398		6	C.847	+27.	5	2.07.0	(n)	7	7	.82	.84	Ξ	5
3	4	4.315	•	7.9	0.866	1.359	ς,	0.830	4.	=	Ę.	7.	.85	Ξ	•
~ 2:	•	4.33	•	.e.	6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00	4. 	٠, ر	206.	45.	9	1.431	.58	رم. د	ζ;	٠, ١
ر ج ج	E	() () () () () () () () () ()		; ?	7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1.682	. 0	200.1	- 4	, (i	1.500	•	e or		
) () ()	? ~	4.261		54	C.927	. ec	٠,	1.200	Š	-	1.629	77	9	1 4	
2	*	4.261		਼ੋ	0.939	.98	٠.	1.300	.27	. 6.4	7.	90.	55	9.	੍ਹ•
Ö	¢	4.273	•	Ġ.	740.0	.13		1.400	3	65	¥B.	66•	.93	~	٠.
23	4 0	4.273	•	. 77	0.956	J	5 (1.500	κ.	90	5.	96	5	5.0	٠,
ر ا	•	4.213	•	ۍ : •	0.060	r	30) 	2	` ·	<u>ن</u> ۔	9 6	5 0	5.	9
3		4.274	•	200	400	היי	, ,	1.10°	υ .	9	71.	2		25-	უ. :
, (• `	707.4			0 C C	706.7	ט כ	006-1	, ~	9 40	. ~	1.592		7 ~	
20	. ~	4.205		. 5.	0.650	40	0	2.000	22	4	3.5	4		2	٠.
0	?	4.170	•	\sim	0.970	.65	C	2.100	.21	.63	6.1.0	52			0
20	٢,	4.125	•	Col	0.971	0	$^{\circ}$	2.20°	6	.61	4.	4		٦.	00.
, 2	~	(8) •	•	S .	2.5.0	\$ 3.	\circ	006.	La. (3	4	1.474			3
<u> </u>	•	\$ \$	•) •	7 6	• 0.0	٠, د	00 4. 7		, i		\$		- 0	200
<u>-</u>	• •	7.5.6		E 7	>	, o c	000-1	00 • 2 0 • 6 0 • 6		•	2 4			יי מיי	ر 2 د
) (. ,				\$25°C	. r.	, ,,,	20.70	. 3		. 4	4,4			00
	. *.	3.61P	•	1.451	0.975	2.565	1.000	2.830	્કે	3.500	2.434	1.4.18		2.374	
000	1	4.750	•	7	926.0	.55	•	≎5 6 €	5	.47	. 4.			.31	00
	٠.	30.10	•	,	925°C	£	\circ	3.000	4	• 45	4	~		÷.	30.
		3.63.6	•	`•	925.0	4	ر	े ं।	at. ≀	44.	7.	4		۳.	3
9 9	۳, ۰		•	4	(a d)	2-450	1.000	3.260	4.4	2 4 4	4 4	1.420		ر. د	90
23	• '	3.175	٠	<u>ئ</u> پ		, , ,	」 ∖	000	י נ		• •	•		•	غ د د
) ·	•	יים - רפיל רפיל ר	•	7.	216.0		, ,	200	7 5	, ,		ر 1		Ġ	ع د
5	-	0	•	_) } }	. 6.3	_	3000	7		r n	,		מַ	3

TABLE 5 7.5 DEGREE SHOCK WAVE GENERATOR

	11 / 11 INF	0.432	75	2	8	84	80 c	60	8	96	5 6	, 0	93	46	0.949	5 6	9	16	5	. 0	98	9	66	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	ő	0	1.030	3 6	3 5	ò	3	00	1.000	000	1.000	8	1.000
٥.	RHOU /	0.381	50	9	9	5	6,	9 4	7	7	~ ;	C 6	9 00	6	5	5	ς c	ŏ	- :	4 7	ŭ	ě	4	4 4	ė	0	9	- •	ŗ	· a	0 0	ی م	e	9	1.904	1.910	015-1
x * 82.	U INF	0.000	0.655	2000	0.731	C-747	192.7	20,79	6.805	C.819	0.824	0.634	0.856	C-8-0	0.819	C. 891	2 C	6.913	C. 920	1 26 0	0,46	0.946	0.952	C. 95.7		C.967	0.573	C.972	0.974	0.4.0	- a	T. 0	260	0.00	160.0	146.0	0.582
ERATOR,	1 / T INF	4.252	3.50	3.205	3.292	3.318	3.297	3, 239	3,03	2.942	566.5	2.854	2.711	2.584	2.507	2.384	2.324	2.200	2-134	2.055	1.924	1.871	1.800	1.728	1.602	1.577	1.536	1.457	1.463	775.1	204°	1.000	1 • 1 C C	1.244	346 1	1.332	1.376
HAVE GEN	RHO / RHC INF	0.656	691.3	148.0	0.003	0.825	C. 831	0.845	0.89	C.931	C.932	C.956		1.040	1.056	1.091	1.120	1.198	1.241	1.289	1.335	1-4-21	1.471	1.519	195.1	1.654	1.709	1.753	1.794	1.831	1.8.1	F - C - C - C - C - C - C - C - C - C -	114.1	0.4.0	1.90	1.946	\$ 9 6
EE SHOCK	P /	2.739	2.73	2.13	2.13	2.13	2.13	2-13	2,13	2.73	2.13	2.12	2.71	2.46	2.64	2.60	2.60	2.63	2.64	2.64	7.6	2.6.5	2.6	2.6	2.6.	7	2.67	2.6.	2.6	7 ° ¢	7 · ¢	7	2 • ¢	7	7	, ,	, J
7.5 CEGRE	x	222.2	2.330	2.592	2.634	2.749	218.2	2.963	20.6	3,205	3,225	3.311	3.424	3 4 4 0 0	3.724	3.869	3.951	4-129	4.223	4.340	764.4	4.638	4.158	4.883	595.7	F 1 1 - C	5.249	828-5	2.400	5.48C	5.535	5.575	5.61.7	5.647	7.0.0	0 0 0 W	
,	Y (CM)	0,0	0.030					1				•	•		•	•		•		1.500	•		٠.	2.000		•				•	•	٠	•	•	•	•	•
	11 / 11 1NF	45.0	0.134	6.2	8	~ ~	8	8	9	E G	o oc	9	5	5	, 0	9	6	ŏò	6	6	õ	م م	ď	ŏ	ŏ	ું હે	ŏ	ŏ	ં	ō.	õ	ó	Ō	Õ	3	0	٠
I	- ž			2	58) ရ (၂)	2.5	25	76	~ 0	ם מער	6	5.1	60 ·	5.4	. 5	73	1 5 2	366	464	534	119,	752	824	895	9.6	- -	2	6	4٠]	921	5 4 1	145	051	150	251	121
0	PHCU	00.0	0.523	0.66	9 !	5 0	0	0.1	~ ·		0 °C	0.8	6.0	٠. ن		•	=	<u>.</u>	-	: -		<u>.</u>	<u>.</u> _	-	-	٠, ٠	7 ~	~		2.	2.1	2 • 1	2.	2.	Γ.I.	~	?
	U / B	000	0.535 G.35C	701	716	731	150	165	781	767	100	8 22 (6836	158	864	. 883	868	500	414	932	5€ 5	747	4 7 4	963	196	375	27.5	3	916	116	116	678	97P	978	613	£ 1.7	970
ERATOR, X × 78.0	T / U / T INF B	252 0.000	535	389 0.701	333 6.716 (256 6.731 (326 0.150	267 0.769	208 6.781 (129 C-794 (C52 C-804 (936 0.822 (787 C.839 (101 0.851	592 0.864	6.883 6.883	324 0.895	233 0.905	359 0.923	.c67 C.932	.843 C.434	.816 G.947	10000	632 0.963	.577 0.967	532 0.570	276-0 105.	515.0 75.4	67.6	417 0.977	.405 C.977	.397 3.678	18G 0.578	386 C.978	386 0.578	380 0.579	311 3.979
HAVE GENERATOR. X = 78.C	RHC / T / U /	C*754 4*252 0*000 C	936 0.535 C	946 3.389 C.701 C	961 3.333 C.716 C	972 3.296 C.731 C	0043 3 3434 CA150 0040	977 3.267 6.769	995 3.208 C.781 C	G17 3.129 C.794	C42 3.C52 C.BC4	CAC 2.936 C.822 (134 2.787 C.839 (161 2.701 C.851	197 2.592 0.864	22 22 22 22 22 22 22 22 22 22 22 22 22	310 2-324 6-895	371 2.233 0.905	421 2-136 C-314	571 1.967 0.932	433 1.843 C.934	702 1.816 0.947	174 1.142 0.933	00.00 Leach 1.00.3	96.0 1.577 6.967	.017 1-532 0-570	0.50 1.50 0.		7.	157 1.417 0.977	176 1.405 0.977	154 1.393 0.678	193 1-189 C.578	.148 1.386 C.978	.19P 1.386 3.578	.194 1.380 0.979	131 3.979
SHECK MAVE GENERATOR. X × 78.0	P RHC (T / U / P INF HC [NF R	205 0.754 4.252 0.000 0	654 4.90C 0.535 C	205 5-946 3-389 C-701 C	2C5 C.561 3.333 C.716 C	265 0.972 3.296 C.731 C	0.00 0.00 0.000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	193 0.977 3.267 0.769 0	193 6.995 3.208 6.781	182 1.617 3.129 C.794	187 1.042 3.052 0.804 (170 1.080 2.936 C.822 (159 1-134 2-787 C-839 (136 1.161 2.701 C.851	102 1-197 2-592 C-864	2000 0 587° 2 27° 1 500 0 500	C45 1-310 2-324 C-895	C68 1.371 2.233 C.905	18.0 18.42	091 1.571 1.967 0.932	691 1.533 1.893 6.939	Cc1 1.702 1.816 0.947	100 1.74 1.72 0.904	# 90 P P P P P P P P P P P P P P P P P P	1963 1.577 0.967	.091 2.017 1.532 0.570	278-2 108-1 108-2 C-875-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CTC	165 164 1647 0.977	CS7 2-176 1-405 0-977	157 7.154 1.393 0.678	345 2-193 1-189 0-578	C45 2.149 1.386 C.978	C46 2.19P 1.386 3.978	.C34 0.194 1.386 0.977	.011 2.196 1.371 3.979
HAVE GENERATOR. X = 78.C	M P RHC T / U / B B B B B B B B B B	C.000 3.205 C.754 4.252 0.000	205 0.654 4.900 0.535 0.555 0.555	2,552 3,205 0,946 3,389 0,701 0	2.632 3.205 C.961 3.333 C.716 C	2.649 3.205 0.672 3.296 0.731 0	2.110 2.213 0.454 0.454 0.154	2,954 3,153 0,977 3,267 0,750	2,426 3,193 6,595 3,208 6,781 6	3.011 3.182 1.017 3.129 C.794 (3.cag 3.182 1.042 3.052 0.804	3 2 1 3 3 1 1 0 1 1 C B C 2 9 3 6 C 8 2 2 (3,312 3,159 1,134 2,787 C.839 (3.475 3.136 1.161 2.701 C.851 (3,549 3,102 1,197 2,592 C,864	(100°) 5°7°(27°1 10°0° 10°°	3.434 3.045 1.310 2.324 0.895	4.C59 3.C68 1.371 2.233 C.905	11. 3 3. (3c 1.42) 24.21 3. (3c) 4. (4.14)	4.516 3.041 1.501 (.007) 01.27 4.456 4.091 1.571 1.967 0.932	4.579 3.091 1.533 1.893 0.939	4.711 3.Cc1 1.702 1.816 0.947	4.846 3.091 1.74 1.74 1.456 0.504	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5.164 3.691 1.960 1.577 0.967	5.25c 3.091 2.017 1.532 0.570	5.971 3.041 2.059 1.501 0.972		0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000	7.6-5 7.1-5 1.5-5	4 4 1 3 057 2 176 1-405 0-977	6,457 3,057 2,154 1,393 C-978	5.567 3.045 2.193 1.384 0.478	5.576 3.C45 2.148 1.386 C.978	5.975 3.045 2.19P 1.386 3.978	5,584 3,034 2,194 1,380 0,577	5.610 3.011 2.176 1.371 3.979

TABLE 5 - CONCLUDED

	7.5 CEGREE	SHOCK	DAVE GEN	ENFRATOR,	X = 86	0.	
A ECM)	1	P / P	RHG /	1 / 1 INF) U	RHOU / RHOU INS	11 / 11 1NF
		,	Ç	,	Ç	Ċ	7
3	3 (9 0	,	3 0	3 4	3 4	7
S	8	87	•	70.	,	7	
0	2	97	3 3	9	9 4	2 4	- ^
2	56	97	9	7	0 1	,	. 0
12	=	₹.	7	7	7.5	5.	90
15	8 1	.28	, 71	. 18	7	R.	83
_	8 5	.26	. 7.1	1.8	,76	5.4	. 84
20	0	28	72	16	77	. 55	95
1 5		28		60	78	5.8	. 87
, 6		28	74	90.	19	59	8 A
	2 -	2.8	,	76.	. 8	. 62	68
9	26	28	79	.87	.82	65	90
		28	. 8 1	.19	83	.68	16
S	4	28	.84	.7.1	. 84	۲.	6.
	.5	28	83	. 59	85	.75	95
2 -		~	9.	η. 1.	86	. 78	65
2	-	28	6	4.	9.	.80	45
2 0		25	. 93	.39	88	.83	4
2	, ,	, ,	55	33	8	85	.95
] -	Č	200	9	2	0.6	.88	. 95
		22	7	. 19	9	. 92	96.
2 ~		7	0	-	5	\$ 5	96.
3		,	5	ું	92	90.	.97
5.5		23		٠. د	9.	. C2	.97
9	. 45	23	. 13	96.	93	0	6.
2	5	.23	- 1	06.	6	.10	Š.
α.	9	.23	.20	.85	.94	=	86.
9	. 12	.23	.24	. ac	46	. 1.	86
3	.82	.22	.21	7.	ę	. 2.	96
$\frac{2}{\cdot}$	25.	12.	• 30	• 69	7.	47	6
7	2	. 20	. 35	.63	96	57.	6
0.	=	.20	,3,	• 59	ě.	32	66
	25.	22.	<u>.</u>	. 55	96.	6	יינט פיינט
5.	. Z	٠,٧	4	.5	5	3 .	<i>y</i> (
3	.3	۶۲.	4.	7	5	4	
~	4	~	.52	7	5	*	9
9	.5	51.	3	7.	6.	.5	٠
6	š		e.	. 38	6	5	9
S	49.	÷.	, k.	. 35	5	.5	9
	9	÷.	9	9	Š	9.	ب د
~	7	-	•	•32	36.	9.	o i
~	٠,	•	1.617	1.315	C#5*)	1.647	1.000
3	7.	17.	₹.	. 29	36.	9	3
3.500	5.872	2.216	.72	.28	ŏ.	9.	င်

TABLE 6 15 DEGREE SHOCK WAVE GENERATOR

	TT / TT INF	•	• 7		٠.	0.761	٠.	٠.	~	•	•	~ ~	. ~	~	~	•	•	. ~		٠.	•	•			٧.	٠.	·ς ·	, •	. 0	O	ب	Ç	٠,	Ö	O	0		1.000
3E C) So	RHOL /	ပ္ .	-	-	٦,	0.175	Ä	Š	~	~	7	, ,	2	, 3.	e,	, e	7	4	*	3	'n.	, 4	9	~	76	e i	80.0	, ,	v	9	6	٠,	3	2			00	$^{\circ}$
X = 25.5	U / U	ŏ		'n	9	0.652	Š	~	~	ř.,	٠,		7	8	60	Ď	ນີ້	8	96	6.	9	, 0	5	96	6	80	20 C	. 0	65	0,	9	8	00	3	00	3	8	S
RATOR.	T INF	्रेंच्	70	ထ	30	3.820	3	4	34	~:		ن د	ä	Ξ.	٠,	4	,	-	ŏ	9	2	9	1.450	• 36	.27	5	1.121	2.0	20.	1.014	1.604	1.362	1.000	1.000	1.000	1.300	1.000	000-1
WAVE GENE	RHO / RHC INF	•		•	•	0.268			•	•	•	•		"	•	•	, ,		٠.				. •	~	Γ.	æ,	20 U		٠,	σ.	σ.	Ċ.	9	\circ	\circ	1.000	C	O
SHOCK	p / d	9	ò	0	ö	1.023	Ö	0	0	9	ر ر	, ö	3	š	õ	٠ ١	5 6	ŏ	0	3	000	ں ر	0	3	00.	0	200		00.	00.	<u>ာ</u>	20.	္ပ	င္ပ	00.	00.	8	8
5 DEGREE	I	~ `		٠.	•	2.288		ĭ	•	۳,	•	•			• •	•		,,,		٠, ١	- 0				٠,	∹'	-1 V	9	Ξ.	æ	an.	∞.	æ	æ	æ	€	a)	æ
-	Y (CM)	•			•	0.150			•	•	```				~``	•				٠.				٧.	٠.	Ξ,	7		۳.	0	_	T C	7	c.	~	N	~	4
							_	_			•							_				_	_	_		_	_	_	_	_	_	_	-	_	_	-	_	_
	11 / 11 INF	٠,٠	9	-	'n,	0.807	8	80	80	ထွင်		ě	Œ	ě	œ c	ž	Ó	6	6.	o (, 0	36	6	9	6	9	, ,	0	٠	1.000	9	3	3	0	ဒ	300°	S	ဒ
1		*•0 000•	124 0.6	.144 0.7	153 0.7	0 0	191	.192 0.8	.2C2 0.8	.213 0.8	257 O B	246 0.86	256 0.87	.28C 0.8E	305 0.89		364 0.92	416 0.91	451 0.94	16.0 B84.	56.0	36.0 327	666 0.98	716 0.99	775 0.99	.824 0.99		00-1 285	963 1.00	Sec 1.00	956 1.30	000 1.00	co-1 000	00.1 000	000 1.00	300 1.00	ccc 1.03	000 1.00
X = 20.0 CM	RHOU / IT HCL INF IT I	*•0 000•	540 0-124 0-6	.598 0.144 0.7	.638 C.153 0.7	.665 J.164 U.7	8-0 191-0 6-8	.113 0.192 0.83	.727 C.2C2 0.8	.741 0.213 0.8	**************************************	776 0.246 0.86	7.4 0.256 0.87	. £14 C. 28C C. A £	.833 0.3C5 0.RG		6.0 6.3 C. 3.64 0.95	.89h 0.416 0.97	,910 0.451 0.94	.523 0.488 0.95	25.0	36.0 129.0 655	967 0.666 0.98	975 0-716 0-99	982 0.175 0.99	0.93 0.824 0.93 0.93 0.93	00 - 335 0 565.	00-1 765-0 765	. 998 C.963 1.UC	.999 C•sec 1.00	000 0.995 1.00	1.000	000 1.000 DOO	00:1 000:1 000	000 1.000 1.00	1.300 1.00	con 1.ccc 1.co	1.000 1.00
RATOR, X = 20.0	U / RHGU / TT INF RHCL INF TT I	.430 0.000 0.000 0.4.	.357 C.546 C.124 O.6	155 0.598 0.144 0.7	.171 C-638 C-153 O-7	64 C.663 Jale4 C.79	.834 C.694 C.1P1 0.81	.769 C.713 0.192 0.82	.610 0.727 0.202 0.8	368 C-741 C-213 O-83		233 0.776 0.240 0.86	.168 0.704 0.256 0.87	.911 C.£14 C.28C O.8E	.732 0.833 0.3C5 0.8c	. Jet	263 C.683 C.884 O.92	153 C.89h 0.416 0.97	.016 0.910 0.451 0.94	.854 C.523 C.48B C.95	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	36.0 129.0 6.65.0 3.65.	.453 C.967 G.666 0.98	362 6.975 6.716 0.99	265 0.982 0.775 0.99	.159 C.588 J.824 C.95		00-1 (0-6-3) (0-6-3)	00.1 6.948 6.963 1.00	00°1 085°0 666°0 5	.035 1.000 C.955 1.30	.0Cc 1.300 1.0Cc 1.0u	00.1 000.1 000.1 000.	00°1 00°1 00°1 00°	00.1 000.1 000.1 000.	.coc 1.cco 1.3cc 1.3c	.00a 1.0 0 0 1.000 1.03	.aca 1.00a 1.0c0 1.uo
GENERATOR, X = 20.0	/ U / RHOU / IT	22.5 4.43G 0.000 0.000 0.44.	-230 4-357 C-546 C-124 0.66	-241 4-155 6-598 0-144 0-7	-2.59 4.171 C.638 C.153 C.7	3.568 0.663 0.164 0.76 3.568 0.679 0.171 0.80	.201 3.834 C.694 C.1P1 0.81	.275 3.7C9 6.713 0.192 0.83	.277 3.61C C.727 C.2C2 O.8	25 3.48G C.741 C.213 O.83	000 7777 CVL 0 0567 CC74	.309 3.233 C.776 C.24C C.86	.322 2.108 0.774 0.256 0.87	•344 ?•911 C•£14 C•28C O•8E	356 2.732 0.833 0.3C5 0.89	41) 2 631 C 446 C 6435 C 644	16.0 5000 16.00 15.4.2 314.	.465 2.153 0.896 0.416 0.91	.45c 2.016 C.910 0.451 0.94	.578 1.894 0.923 0.488 0.95	1007 1707 0 0070 0 0070 0 0070 0070 007	049 1.545 C.454 C.621 0.95	.689 1.453 C.967 0.666 0.98	.734 1.362 C.975 C.716 0.99	.789 1.269 0.982 0.775 0.99	.834 1-199 C.588 J.824 C.99		741 1.064 C.997 G.937 1.00	.964 1.037 C.998 C.963 1.UC	.981 1.016 0.999 0.586 1.00	.595 1.035 1.000 C.955 1.30	.636 1.066 1.300 1.066 1.0u	.oco 1.ccc 1.ooJ 1.occ 1.co	.030 1.000 1.003 1.000 1.00	00*1 000*1 000*1 000*1 000*	00.1 000.1 000 1.000 1.000	00 1.000 1.000 1.000 1.00	00 1.000 1.000 1.000 1.00
SHOCK MAVE GENERATOR, X = 20.0	PHC / I / U / RHOU / III	22.5 4.43G 0.000 0.000 0.44.	.000 C.230 4.357 C.540 C.124 O.66	.Cau 6.241 4.155 0.598 0.144 0.7	-COC C2 59 4.171 C.638 C.153 O.7	• CCC	.000 0.201 3.834 0.694 C.101 0.81	.000 C.275 3.769 G.713 0.192 0.82	.000 0.277 3.610 0.727 0.202 0.83	-crr c.xxx 3-486 C.741 0-213 0-83	000 0 000 0 000 0 000 0 000 0 000 0 000 0	000 0.309 0.739 0.776 0.240 0.86	.000 0.322 2.108 0.774 0.256 0.87	.CCC 0.344 2.911 C.614 C.28C 0.86	.COC 0.356 2.732 0.833 0.3C5 0.89	10°0 0 73°0 0 73°0 0 75	20 0.436 2.253 C.635 C.326 O.525	.000 0.465 2.153 0.896 0.416 0.93	30 C.496 2.016 C.910 0.451 0.94	-UCC C.578 1.854 C.523 C.488 C.55	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 0.6548 1.5458 0.459 0.621 0.95	10 C.689 1.453 0.967 0.666 0.98	30 0.734 1.362 C.975 C.716 0.99	33 C.789 1.269 0.982 0.775 0.99	00 C.834 1.199 C.588 0.824 C.99	00 - 0	00-1 1-00 00-00 1-00 00-00-00 00-00-00 00-00-00-00-00-00-	0.964 1.337 C.998 C.963 1.00	00°1 085°0 666°0 510°1 185°0 0°	00.1 888 1.005 1.000 0.988 1.00	00 1.636 1.066 1.300 1.066 1.0u	00.1 000.1 000.1 000.1 000.1 0:	00 1.030 1.000 1.000 1.000 1.00	00-1 000-1 000-1 000-1 000-1 00	. 1.000 1.000 1.000 1.000 1.000	:c 1:000 1:000 1:000 1:000	0 :- 000 1.000 1.000 1.000 1.00
MAVE GENERATOR, X = 20.0	P / PHC / T / U / RHOU / TT	CCC 0.226 4.430 0.000 0.000 0.000	.777 1.0CC C.230 4.357 C.540 C.124 0.66	.C13 1.C0c 6.241 4.155 0.598 0.144 0.7	1.42 1.00C C.239 4.171 C.638 C.153 O.7	.283	.434 1.000 0.201 3.834 0.694 C.1P1 0.81	.541 1.000 0.275 3.709 0.713 0.192 0.82	.627 1.000 0.277 3.610 0.727 0.202 0.83	1.40 [1.40] [1.4	1914 1:000 0:030 0	38.0 0.42.0 0.47.0 0.85.3 0.47.0 0.00.1 0.49.	.052 1.000 0.352 2.108 0.774 0.256 0.81	274 1.000 0.344 2.911 0.614 0.280 0.86	436 1.000 0.356 2.732 0.833 0.305 0.89	1634 1-000 (-3)3 2-360 (-630 0-130 0	76.0 0.65.0 16.03 15.43 3 15.03 0.031 336. 0.436	189 1.000 0.465 2.153 0.896 0.416 0.91	35e 1.ccù c.45e 2.016 c.910 0.451 0.94	663 1-506 C-578 1-854 C-523 C-488 C-55	0	243 [.CCC 0.648].545 C.459 U.650	50e 1.000 0.689 1.453 0.967 0.666 0.98	735 1.0C0 0.734 1.362 C.975 C.716 0.99	585 1.CCC C.789 1.265 0.982 0.775 0.99	1.66 1.000 L.834 1.159 C.583 J.824 C.95	20	1 1 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	724 1.000 0.964 1.031 0.998 0.963 1.00	385 1.500 0.581 1.019 0.999 0.580 1.00	842 1.00 0.545 1.005 1.000 0.955 1.00	PA1 1.600 1.600 1.000 1.300 1.000 1.00	861 1.600 1.600 1.600 1.000 1.000 1.60	861 1.000 1.000 1.000 1.000 1.000 1.00	00*1 200*1 1*00*1 700*1 1*00 1*00¢ 1*00	Pet 1.00J 1.00A 1.00C 1.00G 1.00C 1.00	861 1.000 1.000 1.000 1.000 1.000	861 1.668 1.000 1.000 1.000 1.000 1.00

TABLE 6

	15 DEGREE	E SHGCK	MAVE GENE	RATCR,	x = 24.	. O.		-	S DEGREE	SHECK	MAVE GENER	RATOR,	X = 3C.5	F C F	
Y (CM)	I	ō.	RHC /	\ <u>+</u>	\ D	RHCU /	/ 11	YICH)	1	7 d d	AHO /	1 / T	י ט מ מי	AHOU /	\ <u>11</u>
		-	_	 		2	2			•	2	:	•) }	
ć (,	. 7.2	S	4.2	00000	0,00	43	Ö	0	, 2 C	12	42	_	200.0	0.432
0		,	0.3	2	0.213	0.07	24	Ö,	- ·	20	5.	5	3 6	Š	
0.075	0.800	1.765	0.324	5.251	0.269	C = C 8 J	C, 580	0.075	2540	3.465	175.7	- T T T T	200		
0.100	۲.	7.	ر ک	28	0.331	01.0	٠ د		<u>-</u> ۳	, כ	4	2	3 6	40	
0.125	-:	σ	ပ်	. ي	C . 38C	21.0	5		4 -	3 0	4	. 4	3 2	5	
0.140	1.2	T)	<u>.</u> ت	3	0.424	61.0	0 6		<u>،</u> س	, ,	4	9	. *	ဗိ	
0.175	4.1	۲,	(,	, G	· • • • • • • • • • • • • • • • • • • •	2 0	7 7		. 4	3 .		96	-	0.8	
C 05.0	. 5	s.	ر در	ر ان	0.00	9 0	- 1	• ^		25		85	21	0	
C. 250	τυ (1	، د	- 7	1.00 C	2 6	٠,	-	٠	22.		13	.24	-	0.718
008.0	-	v) (2 6	0.645	2.2	19		_	25		7,	28	13	
	, . , .	צ כ		-	0.666	0.25	63	-2	=	25		9	0.	5	
) (, .	o w	• [. 0	289.7	0.27	8	4	œ	2 c		48	34	_	
) (* * ·)	, ,	٠.		7	0.711	0.28	82	4	9	, 2C		8		2	
) () () (, ,			1	0.150	0.32	8	4	∹	5 0		7	7,	7	
) () () () () () () () () () (•	7	-	C. 784	C.35	86	٦.	\sim	2		7.	5	5	797.0
				5	0.813	0.38	88	-	₹.	22.		=		2 6	
1000				6	C. 838	0.41	8	٠,	ς.	.20		, 26	. 5.	Ę.	
•	, ,			3	0.860	0.44	9	٧.	5	.20		- E	69	3	0.830
)	1 4		ن	, , e	0.879	0.46	92	٦.	~	,20		26	9	٠, روا	
) (_	d	-	0.850	0.46	6	•	ŭ,	22.		٥.	٦.	ت	400
		9	, ()	,	C.913	0.50	ó		"	25.		9	-	9	
		2	7	-8	6.929	0.53	6	٧.	۳.	25.		4.		7;	0.0
			(c)	8	0.941	C.56	9	٠.	9	20		~ ;	æ :	9 6	11000
		ر	3	9	566.0	0.5		•	ુ	20		5	26.		264.0
702-1	, , ,		٠ ن	5.2	6.561	0.62	٠.		٦.	200	0.576	62.	ည်းငဲ	. G	2.00
20 8 - 1		ੰ	,	3	6.96.0	0		٠, ١	7.	7,		, כם י	9	9 4	0.00
1.930	s)	9	ڻ	.38	5.615	~ ·		•	, .	,		7		3	0.977
2.000		Š	0	<u>ج</u> :	386.0	ن ن د		-	•				98	8	0.0H4
2.100		~ i	، د	7		, a				20		.05	.87	6	0.989
2.200		ວ່ ຄ	3 (-	3000	, 70 , 0			•	- 20		5	88.	5	-
70.0		ું ે	_، ر	Ü	366.0	6.0		٦,	٠.	5		5.	5	~	0.995
7 7 W	•	į č	•		6.998	5		-	٦.	5		. 3.1	.92	Ř.	
2,000	•	ć	; (,		656.0	3		٠.	٠.	. 12		0	5.	4	<u> </u>
\	. 4		, ,	ŏ	1.000	6.0		٠.	٠.	٠. ب		6		7	٠, .
107			, -	Ö	1.000	1.0		٦,	٠.	9.		ée	0, 1	ပ် (000.1
		Ú	_	ŏ	1.000			٠.	٠.	9		20 0		,	000
• •		3	~	਼	1.000	j.		•	~∵	<u>.</u>		200	,	5	300
		Ö		ŏ	ു റാ - 1	٠ <u>٠</u>	1.000		•			90	C	9 6	
3.200		ŏ	_	7	1.000	Ö	000.1	•	•			9	, G		
((1))	٠	~	-1	ć.	1.000	0	000-1	•	~ `	77.		- G		- 0	1.000
004.0	Ų	Ö		٠ ٠ ٠	1.300		2000	•	•						_
3.530		õ	<u>:</u>	ŏ	00 0 • 1	-	200	•	•	•		; ;	`		

:7

ORIGINAL PAGE IS OF POOR QUALITY

TABLE 6

	11 / 11 INF	0.432	~ ~	~ •	. 60	ص ون	æ	۵. ه	စ်ဆ	æ	<u>م</u>	0		~	٥.	م د	20	ુ	9	9 9	0	0	၁၀	20	0	0,	2 (, ()	0	9	9	9	
.	RHCU /	0.0000	117	• 1.4 • 1.4	91.	.21	•26	• 28 33	35	.43	53	2		.37	• 55	900	83	36.	55.			. 54	- S	50	.20	.30	• 2. c		33	.02	ď	36.	46.	٠,٠
x = 35.5)))) ANI	0.000		.2	3.6	~ ~	4.	3 4	, r.	S.	9,	۰۰	- 00		σ,	ۍ د		0	5.	. J		o.	ຽຸ		5	σ,	• 2. C	ָיי.	٠,	٠,	•	6.	6,	•
KATÜR,	T / INF	4.426	7.642	7.637	7.453	7.328	1,00.1	6.846	6.36.9	5.892	5.345	4.712	30102	2.75	2.457	512-7	010.0	1.719	1.623	714.1	1.767	016.1	2.037	2.318	2.430	504.2	9,4.7	2-133	565.1	1.566	1.531	1.924	7.12.) 1
AVE GENEK	RHC / FHG INF	1.027	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	565.0	0.631	0.620	649	499.0	017.)	(.171	C - 85C	€35.4 - 5.5 - 6.7 - 7.5 - 7.5	201.1	1.565	1 702	1.767	1.920	1.933	2.006	2.2.1	2.476	2.677	2.501	3, 134	3.484	3.598	3.642	3,000	6.04	2.138	2 • C # 9	2.007	2.045	2.163
SHCCK	P /	4.545	N. N.	3	4.0	4 4	3.	.54		5.	5.	4	40.	.37	2	36	5.5	4.0	. 35	3.4	7.	=	36.	. 72	4.	5.	ָרָי לָּי פּירָי			0	Ş	5.	25.	÷.
GENERATOR	I	0.000	4.0		• -	w. 0	•	∹'	, E	9	æ (? "	n c	ur.	5	~:	٠, ۲	9	~	• •	. 5	۲.	٠, ٦	•	ာ	5	٠,	. 4	. 4		9	•	٠.	`.
	4 CH)	050.0	0.100	251-2	0.175 0.200	0.250	0.350	0.4.0	364.3	0.000	001.0	0 8 3 C	ر ان دران ان دران	1.100	1.200	300	C 5 5 1	1.630	1.700	1.800	2.000	2.100	2.200	2.463	2.500	204.5	2.7.0	2000 6	3000	000	3.230	3,300	3.400	2000
SHOCK WAVE	TT /	0.432	0.698	0.710	0.717	C.727 0.727	0.730	C.732	0.735	0.735	5,737	261.0	0.757	0.769	0.792	0.815	0.0	3.886	906.0	755.0	086.0	0.958) () () ()	1.000	1.000	000.1	000		000.1	1.000	1.000	1.000	1.000	T
DEGREE C#	RHOU /	0.00 0.00 1.50	55	2.5	55	င် ပိ	90.	25.5	200	2	25	9 0	,	1.5	. 25		1 .v.	7	7.5	75.	5.	. 75	. 2 .	. ~	2	5	7.5	, ,			~	12.	?	
15 x = 33.0	U INF	0.000	13	7.	<u> </u>	= 2	. 12		80	်	50:	0 		7	.42	.5.		7.	30	a 0	25.	č.	<u>.</u> 5		15.	3		7 V	٠,٠	25	9	\$ 5	•	•
RATUR	1 / 1 INF	6.346	86.0	85	3:-	22.	74.	. A.	, 4	.51	. 53	44.	,		,,	. P. S.	, , ,	65	61.	35.	, ,	1	0 4	. 4	S	. 35	· ;		- d	4	I.	Œ.	÷.	•
A YE GENE	RHC / RHG INF	0 9 9 8 9 8 9 9 9 9	0.550 0.550	3.542	0.036	0.532		617.0		C.511	0.510	0.516		0.568	565.5	0.651	2. 125 2. 824	505.7	1.233	0 10	2.769	75).5	က် မ	, , , , , , , , , , , , , , , , , , ,	404.4	. 11.	000 4	, c	7 T	. 45.	2.4.5	4 4 E - 3	846	2 - 41 4
SPCCK N	P INF	3.00	9 4	4		4 4	4	4 .	7 4	4	4	47	7 4 0 7	4	47	4	4 4	4	4	4 C	· *	. 0	♥) ♥		2	5	د د		۔ ر		α,	-	~ .	-
CEGREE		000000000000000000000000000000000000000		0.1±2	C.36.2	C.351	906.0	0.213	5.23 S	0.145	C. 130	108.0	7.4.7	7 7	1.165	1.457	72.1.0	466.4	3-122	3.157	251.4	**255	£.013		3.855	*. 1 .	410.4	C , c	1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		, , , , ,	4.7.6	4.78%	4 - 7 = 3
ž.,	A ICM)	0000		:2:	- 2	25		9	4 m	9	7.0	3	3 5	2 -	2	2	د د		٠ ٠	و د	200	2	2) (ć	`.'	g i	; 6	-		<u>-</u>	4	?

TABLE 6

	19 DECREE	SHCCR	HAVE GENE	RATCR.	× = 38.	1 O		~	S CEGREE	SFOCK	MAVE GENE	GENERATOR,	× = 40.0	Š	
(W) A	x	7 0 0	RHC /	1 / T	U INF	AHGU /	11 / 11 1NF	Y (CH)	•	P / P	RHC / RHO INF	1 / 1 1 NF	0 / 0 0 INF	RHOU /	17 / 17 INF
000	c	=	-	4.2	8		43	0	2	4.	1.905	4-426	00000	0.000	0.432
0.00.0	1.239	6.761	-	5.845	0.430	0.504	0.744	0.050	1.231	281-8	1.232	6.550		9	0.852
3.075	1.2	2	.	6.	2 1 2 1		2.5	5 2	9	Š	1.241	7	5	63	0.859
001-0	7	# 0	<u>.</u> -	2 .	•		. 2	2	43	.89	1.244	¥.		\$ 5	0.867
, , , , , , , , , , , , , , , , , , ,	-		-	6.020	4		5	2	4	9	1.248	2	n 4	- 9	7 0
0.175	-	. 0		9	4		8		25	- 6	1.250	-	7	7	0.882
202	_	4		5.871	3		80	25	9 4	7	1.279	. 0	Ś	- 2	0.840
2.250		38	-	5.623	a . ,		z	2 0	5	20	1.315	2	•	.	C-847
0.400	-	2		5.381	2 4		3	, ~	6	4	1.386		¥	3.	606.0
0.350		~	<u>.</u> .). I. c	7		6	, 3	6	38	1.442	. 12	•	5	215.0
ວດ ••ງ		_ :	٠.	י פ	3 3		ê	5	1		1.447	8	•	ö	0.920
0.84.0	.,	_ 3	÷-	77 7	9		Ď	20	33	.2	1.573	79	- 1	-	0.932
30 5 3	•	٦ ر		5	, -		96	9	c)	7	1.761	٠ ا	۰,	•	26.0
3 c	• ~	٠,	. , .	2.850	<u>_</u>		.88	2	7	ŏ	2.095	ř.	D 0		0.00
	, –	. &	~	2.311	ĕ		26.	8	9	0	044.7	9 -	9 0	-	1.01
	,	5	~	٠.	Š		92	36	7	Ξ,	7.094	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	. 0	ŏ	1.023
	;	~	·	* 7	o i		•	<u>ځ</u> ک	,	- 0	3.179	5	σ	ŏ	1.023
1.100	;	3	, -	ř.	5		. 0	3 6	0	3	3.108	~	96	ĕ	1.015
1.236	•	ŏ.	, i	£ :	> 0		. 0	, ~	ò	æ	2.801	ř.	96	2.693	1.003
700	<u>.</u>	-	, -	•	ð		00	¥	Š	Ö	2.361	•	96	7	1.000
004.1		ہ نہ	-		U		00.	3	7	₹.		ğ.	8	ه ره	000
) (•	•		. 51	o		60.	9				• •	2 0		000
· · · ·	• ;	Œ.	_	1.509	0		င္က	۲ ;	7	, 0			. 6	1.776	1.000
	•	ũ		. 55	œ		3	ã	7 7	Ď .		٠,	3	1.787	1,000
1.930	•	ř.	~	1.615	ŏ, d		י פיק	Ď		0		ě	9	1.918	1.000
2.036	•	٠٠٠	ru e	ò :	ř		,	<u> </u>	-	=		9	96	1.852	200.1
001.0	; .	اب	'4 ()	707.1	Ò		1.000	7	0	Ť.	1.969	1.702	C.962	1.894 1.00	1.000
7.200		. 4		8	ۍ		00	ě,	δ,	v.		•	2 0	- 60.	000-1
		~	•	\$	Ġ.		\circ	4	. r	- 0		• •		2.026	1.000
2.500	•	~	•	S.	ġ,		\circ	ñ 3	. ~			6	ō	2.075	1.000
7.643	÷	٠.		71.	•			7	٧	'n		o.	5	2.131	1.000
2.70	÷	w ·	~ .	7 ×	יַי) (œ	Š	9		ŏ.	ŏ.	2.184	1.000
2.800	;	٠, ٠	•		. "		9	õ	÷	~		0	ġ.	2.22.0	>
006.7	;	٠, ٠	۷,				\circ	Õ	4	ن		0	ŏ,	2.271	
ုင်ပ (၁) (၈)	;	``	•		5		O	Ē	4	7		<u> </u>	> 0	2.314	3 8
0.1.6		• ~	٠,		9.		•	~	'n	٠,		∹.	ن ج	7 376	
37.5	; .	•	. •	Ö		0	000.1	3.300	ď.	4.			, 0	2.408	30
) () () () () () () () () () () () () ()	•	•	. ~	.89	٠,		1.000	3.400	4	4 0		• (Ö	7.343	1.000
0000	;			1.900	٥.	.59	0	3.500	Ñ	•		•		1 1	ı

TABLE 6

	9 CECACE	SHOCK	MAVE GENEP	PATUR,	X = 42.	S CH		1	S DEGREE	SHOCK	MAVE GENE	RATCR.	X = 45.	* 0	
•								# C >	×	۱ م	Ų	1		AHOU /	11
(ROLL		P 1 NF	AHO CAF	- 1 NA	O INF	RHOU INF	TT INF	,		d IN	PHO INF	- IN	∪ 1 NE	RHCU INF	T IN
,	•			7	- 0	C	0.432	0.000	000.0	115.8	2.028	42	000.0	330.3	0.432
3 3	7			2.00	, 4		0.835	0.000	1.706	8.83C	1.493	6	Φ,	•	0000
ŝ	000	7.6	7 4			O	0.861	3.075	1.856	6.761	1.551	5	o,	•	034.0
5 9			74.			J	0.870	C. 100	1.891	60°	6.64	9	ο ,	•	4 C
2:			1				0.860	0.125	1.925	8.636	946.		0 4	. 70	0.49
: :	425		4			٠	0.886	0.150	1.557	8.591	1.73	1	9 4	4 (4 ()	0.042
	1.568	6	***		•	_	0.892	541.0	155.	4.00	1.565	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1.076	0.942
	1.626	6.86			•	•	668.0	0.203	2.023	, de	1621	1	, ~	1,135	0.943
3 5	1.733	8.71	1 . A		•	_	906-0	267.0	21	9000	1.657		. ~	1.182	946.0
30	1.636	6.58	1.51		•	·	616		2.281	8-227	1.708	2	~	1.246	0.947
-	1.945	6.47	1.55		•		*76.0	0.00	- F	8-159	1.759	6	~	1.310	0.950
3	2.0e3	6.3			•		0.932	0 0 0 4 0 0 0 0	2.484	8.091	1.824		~	1.391	0.955
,	2.190	8.2	-		- •	_	140	00500	2.551	8.034	1.889	.25	_	1.471	096.3
3	2.335	9.18	-			_	0,00	009-0	2.844	7.932	190.5	.84	æ	1.677	596.0
•	5.069	ပ •	75.				2 4 6	001.0	3.143	7.841	2.285	4.	w	7.64	0.482
Z	3.047	7.86	7.10					008-0	3.482	1.113	2.566	03	w	2.267	266.0
C. BC	3.547	7.1	3 · • •		• `	-	900	206*3	3.754	7.693	2.78C	٠,7	Ψ.	2.531	1.014
ĕ	4.037		5			•	1.028	0001	3.992	7.636	3.0C7	5	v.	2.189	1.020
8	0 4 N	~	7 . 7		•		1.030	1.100	4.212	1.557	3.234	• 33	٠.	3.036	1.020
\simeq	664.4	-			•		1.028	1.200	4.365	7-443	3.404	3	٠.	3.206	1.0.1
~	901		7.6		_		1.625	1.330	4.455	7.273	3.457	~	٠. ١	3.256	* 00 • 1
× :	4.613				•		1.017	704-1	4.503	1.001	3.439	ာ ၁	٠, ١	3.242	700.1
			,		•	_	1.006	1.500	4.547	6.818		3	•	3 0 0	
ŕà		, -			-		1.000	1.630	4.621	6.420	3.252	, 0		2.010	000
ć ~	4.673	3.2	.4		-		0000-	1.700	778-4	720.0	\$ C. C.	-	. •.	2,695	1.000
œ.	5.663	7.5	1.1		-		1.000	1.50	0 - 0 - N	7.677)	- 49	٠.	2.208	1.000
ŏ	56105	2.84	1.7		-		220-1	7000	5.179	5 6 5 5	1.806	1	٠.	1.744	1.00c
Ö	5.1c+	ğ. ?	7 - 7		٠.		000	001.	59165	2.127	1.659	40.	٧.	100.1	1.000
-	*51.6				2			2.200	5.205	2.635	1.026	1.622	٧.	1.571	000.1
~	4.121	- ·					1.000	2.300	5.187	2.670	1.637	1.631	٠.	1.581	000.1
~	(\(\)) ·					1.000	2.40C	6.11.5	2.127	1.667	1.636	٠. ١	1.610	000.1
ě,							1.000	2.500	5-156	2.784	059.1	1 - 6 4 B	`. `	769.	
٠,		•	• •				1.000	2.600	5.134	2 . 8 4 1	1.17	1.66	`.`	1.001) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C
٠ ب	0 0 0	r v	: -				000-1	2.700	5.113	2.85E	1 . 7 34	1.001	`. `	1.0.1	300
` '	70/14		-				1.000	2.80€	2.00.5	2.555	1.756	20 (d)	•	1.0.1	
D,	1 1 P		•				1.000	306°?	5.015	3.C11	977	# 5 C * 1			000
?.′	F) 4 4						000.1	3.000	6.0.3	3-668	909	427.	•	16/-1	
٠.							000.1	001-6	5.043	3.1.4	7 .	7.7.	•	10101	000
) 4 G	, -	, ,				1.000	000.	5.034	3.15	7.8.1	1.15	•		000
		4.261		2.020	0.944	1.992	1.000	30.300	2.011	3.205	1.T.	3 - 1		1.792	000-1
•	4.526	•	7.1		•		1.000	200	r 0 7	306 6	- 0 0 0 0	1 7 5 4	• •	1.802	1.000
205.	145.4	-	7.1				1.000) (• •	000	7.63.5	D	•		!) •	•

TABLE 6 15 DEGREE SHOCK WAVE GENERATOR

	11 / 11 1NF	0.432	0.813	200	0.804	C.881	0.892	0.400	0.934	0.943	156.0	0.456	0.966	7 0	200	0.0	156.0	766.0	156.0	0660	200.1	000	000.1	1.300	1.000	1.000) () () () () () () () () () (1.000	2.00	1.030	1.000	1.00c	1.000	1.300	1.000	1.000	1.000	1.000	
3.	RHOL / RFCU INF	0.000	631.1	1.1.1	1.206	1.216	1.231	1.273	1.321	1.342	1.364	1.388	1.423	1.40E	115.1	1.500	500	1.730	552.1	1.875	1.950	7.0.7	2.133	2.190	2.235	2.276	2.306	2007	7.356	7.356	2.350	2.346	3.346	2.334	2.314	2.296	2.276	2.25€	2.241	
X = 55.0	U INF	0.000	0.724	05/0	2.775	0.184	6.193	608	228.3	C. E37	C.844	C. F 50	0.859	598.0	7.8.7	C. 883	26.04.7	0.905	0.911	0.918	0.923	875.0	1 (F () () () () () () () () ()	C. 534	0.46.0	5.942	445.0	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2 7 7 7 C	0.00	0.951	2,952	0.053	6.953	3.954	6.943	0.943	5550	756.7	
RATOR,	1 / 1 INF	4.426	3.433	3,349	3.346	3.326	3.369	3.263	3.233	3.151	3.166	3.130	3.087	4.324	2.555	2.859	7.73	2.645	2.562	2.476	2.394	2 • 4C 6	0.7.7	7 1 4 5	2.102	390.5	7.322	2.001	C 30	4000	805	1.8886	1.865	1.856	1.850	1.563	1. A. c.	1.873	1.883	
AVE GENER	RHC / RHC [NF	1.212	1.531	1.561	1.556	1.551	1.552	1.574	835.1	1.603	1.616	1.634	1.656	169.1	1.731	1.769		1.912	1.974	2.042	2-112	2.167	2.226	2.3.5	2,379	2.418	2.445	2-470	184.7) a	2.472	2.44.7	104	7.445	7.47	014.7	2000	2.371	1.344	
SHCCK N	P /	5.364					_	_		-									_		Ξ.	_	-	-																
E CEGREE	ı	00000	2.681	=	e c	4 7	5	5	~ :	- 0	4 5	, 2	, m	3	4	an .	ō,	- 0	5	ರ	ŭ	_	~	٠,	1	4	ŵ	4	٠,	ر ن	~ ر	_	^	_ q		. ~	• •	. ~	_	
~	Y (CM)	000	0.075	001.0	0.12	2.2	, O	0.250	0.300	0 (C) (F	00000	0.690	0.100	C.80C	006*3	000.	1.100	2004-1	004.1	1.500	004-1	1.700	008.4	000	000	2.230	2.300	2.436	236-7	200.0	000 C				0 0 0	.02**		3.500	
	U.			_				_	~ •		~		_	ာ	4	00	~ ~ ~	x. ~	· x	~	_	٠ <u>.</u>	٠, ٠	c	ر م ر	0	5	ر.	2:	Ž (_ ر		<u>.</u> ر		- ر	2	: د	2 0	,
	11 / 11 IN	0.432	505°0	0.923	0.932	149.0	3	76.0	0.95	0.00	5 0		95.0	0.97	12.0	C.97	တာ ၈ ၁ (0 C		00.	1.00	- C.	٦٠٠ ١٠٠	٠ • •) (- -		o • ¶	رن - ۱	0.1	5 c) C) ()) c	3 6) C	-		• •	•
Œ.	1 1		درار: 15	243		700	321	356	393	436	· ·	- v	177	74t	95,0	416	114	7.7		647	124	15.4	94C	478	# C	0.00	812	.77:	721	30	710		,	, . ,	172					
X = 50.0 CF	RHGU / TT	220°2 coo	درار: 15	152 1.243	759 1.252	765 1-271	77H 1.321	747 1.350	797 1.393	808 1.436	013 1.473	0.77 1 6.5.	923 12638 838 12638	851 1.746	HE4 1.85C	677 1.974	890 2.114	909 2.271	22. 7.54.	7.047	437 2.729	9-1 2-7-6	348.5 2.846	24.5 C 245.		000 T	2.812	2.172	2.721	2.66.7	2.00.7	0 7		77.0	720) a	C 4) 7 (
* 50.0 C	/ RMGU / TT INF RECU INF TT I	250-0 0000 0-000	739 1.215	248 C-152 1-243	241 6.759 1.252	201 C.765 1.271	13.	022 0.187 1.350	326 0.797 1.393	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	746 0.613 1.473		0.00 C 0.00 L 10.00 C	268 C.851 1-746	Lou Cares 1.850	919 1.877 1.974	773 (2.114	603 0.403 2.27	461 C+414 Z+4.	30.0 C.02.0 2.04.0	22.5 (2.53) 2.729	170 0.941 2.754	123 0.542 2.840	47.00°C C4.00°C O2.00°C	#7 L 1	0000 0 0000 0000 0000 0000 0000 0000 0000	10 Cente 2 812	010 (2445) 2477	344 C.945 2.721	136 C.548 7.661						0 1		047 (040 0 474)		
CENFRATOR, X = 50.0 C	1 1 0 0 8HGU / TT	1.602 4.426 0.000 0.000	1.622 4.645 C.693 1.055	1.653 4.248 0.752 1.243	1.650 4.241 6.759 1.252	[.eo] 4.201 C.765 1.271	1.673 4.137 0.778 1.328	1.715 4.022 0.787 1.350	1.749 3.926 0.797 1.393	1.783 3.831 0.805 1.436	1.011 5.746 0.013 1.473	1.0844 J.601 C.6571 1.01	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7.04. 7.068 0.851 1.746	7.141 3.100 0.864 1.850	2.251 7.938 4.877 1.974	2.376 2.770 C.89C 2.114	2.514 2.603 0.403 7.27	2.655 7.461 C.414 Z.4.7	[40] C C C C C C C C C C C C C C C C C C C	27.5 (c.2) 5.225 (c.2) 7.255	2.464 2.170 6.941 2.794	3.014 2.123 0.542 2.84C	42.00 - 4.00 - 0	またまつ とまびょう まずひさつ ブルジャン	3 C S C S C S C S C S C S C S C S C S C	00000 00000 00000 00000 00000 000000 0000	0.44.0 0.40.0 0.40.0 0.4.4.0	151.0 649.0 496.1 818.5	1997 1988 C.548 2.661										
SHICK MAVE GENERATOR. X = 50.0 C	F INF RHC / T / U / RHCU / TT	220.0 0000 0.426 0.000 0.000	2 4.645 C.693 I-055	1,653 4,248 0,752 1,243	300 1.650 4.241 0.759 1.252	577 [.col 4.20] C.765 [.27]	455 1.673 4.137 0.771 1.675	25 1 25 4 25 0 25 0 25 1 25 C	eck 1.749 3.926 0.797 1.393	610 1.783 1.831 C.KCS 1.436	764 [.81] 3.746 0.813 [.47]	75C 1.844 3.661 C.62.1 1.01	70.7 10.00.77 0.00.4 0.00.7 10.00.6 0.00.7 10.	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.251 2.578 4.877 1.974	5AC 2.370 2.770 C.890 2.114	545 2.514 2.603 0.4003 2.271	6.44 0.4655 0.461 0.4414 2.4477	[49*C	201-12 1-12-12 00-12-1 1-12-12-13-13-13-13-13-13-13-13-13-13-13-13-13-	2.104 2.464 2.170 0.941 2.704	19 3.014 2.123 3.542 2.84C	420 C 645 C 050 C 540 C 446	#74.7 (#5.1) #70.7 7.0.6 (A.7.	CONTRACT STATE OF COMMENTS OF	000	026-44 (323-4) 000-44 (377-4) grs	150 0.445 1.554 0.945 0.721	199.2 845.0 BSS.1 418.7 114.						orania social sector sector social social			CONTRACT OF THE CONTRACT OF TH	
HICK HAVE GENERATOR. X = 50.0 C	F P RHC / T / D / RHGU / TT C INF RHGU / TT I	220.2 600.2 6.426 2.003 6.000	268 1.522 4.645 G.693 1.053	7. C. 3. 1.653 4.248 0.752 1.243	7.000 1.650 4.241 6.759 1.252	c. 477 .e61 4.201 C.765 .471	6.455 1.673 4.157 C.778 1.321	8.55 1.554 4.022 0.787 1.35C	6.864 1.749 3.926 C.797 1.393	5.610 1.783 1.831 C.RC5 1.436	C. 764 1.011 3.746 0.013 1.473	6.150 1.844 3.661 C.621 1.01	6.727 1.0877 4.064 C.0677 1.077	07-10 07-10	7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	6.614 2.251 7.538 1.877 1.974	6.540 2.370 2.770 C.890 2.114	6.545 2.514 2.603 0.903 2.271	0.44. 0.46. 0.46. 0.41.	[#972	22.00 (C.C.) 20.00 (C.C.) 12.00 (C.C.)	454.5 C. 1.45.0 C. 1.1.0 2.7.1	5. 49.4 3.014 2.123 3.542 2.84C	429+0 - 446+0 - 0×0×0 - 3×0×6 - 446/4	サブキャン (まか・) オオロ・ペー・ティロ・ペー・レトペッツ	0.00 (02437 (355) OTO35 (357) GTS (375)	121-6 6-6-6 6-5-6-1 6-6-6-6	199.2 845.0 305.1 418.7 114.4						3883			COMPANY OF THE COMPAN	

TABLE 6

C.000 0.000 3.057 0.591 4.426 0.000 0.005	000 0.000 3.057 0.591 4.426 0.000 0.000 0.005 2.196 3.057 0.550 4.074 0.546 0.046 0.048 3.057 0.550 4.074 0.546 0.046 0.048 3.057 0.683 3.549 0.752 0.485 0.785 3.057 0.685 3.549 0.775 0.685 0.075 0.085 3.057 0.075 0.085 0.075 0.085 0.075 0.085 0.075 0.085 0.075 0.085 0.075 0.085 0.075 0.085 0.075 0.085 0.075 0.085 0.085 0.075 0.085 0.075 0.085 0.085 0.075 0.085 0.085 0.075 0.085 0.085 0.075 0.085 0.	784 0.0	00000000000000000000000000000000000000	479664444444444444444444444444444444444		69 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.050 2.196 3.057 0.750 4.074 0.050 0.055 0.012 0.055	0.050 2.196 3.057 0.863 3.541 0.755 0.653 0.1010 2.754 3.057 0.863 3.546 0.755 0.756 0.755 0.756 0.755 0.756 0.755 0.756 0.757 0.756 0.757 0.757 0.757 0.758 0.757 0.757 0.757 0.757 0.758 0.757	000	000000	00000000000000000000000000000000000000		1.016 4.025 0.055 0.066 1.111 3.0682 0.715 0.066 1.118 3.062 0.742 0.0641 1.118 3.062 0.742 0.0641 1.126 1.1
0.100 0.124 0.757 0.107 0.108	0.124 2.754 3.057 0.863 1.941 0.756 0.663 0.1156 2.768 3.057 0.865 1.565 0.767 0.663 0.767		00000	1	682 C. 742 C. 841 C. 943 C. 943 C. 943 C. 944 C. 94	1.113 3.012 C.742 C.841 1.118 3.006 C.742 C.841 1.118 3.006 C.742 C.842
0.124 2.788 3.657 0.855 3.565 0.757 0.658 0.707 0.665 0.1156 2.4624 3.657 0.855 3.414 0.402 0.719 0.665 0.200 3.687 3.687 3.484 0.779 0.665 0.200 3.687 3.687 3.484 0.779 0.665 0.200 3.687 3.657 0.825 3.414 0.843 0.771 0.659 0.200 3.270 3.657 0.825 3.414 0.843 0.771 0.650 3.270 3.657 0.825 3.201 0.832 0.774 0.856 0.400 3.277 3.657 0.825 3.201 0.832 0.774 0.846 0.650 3.427 3.657 0.825 3.201 0.845 0.825 0.400 3.427 3.657 0.825 3.201 0.845 0.826 0.846 0.845 0.845 0.825 3.414 0.845 0.856 0.846 0.845 0.850 3.427 3.627 1.627 2.979 0.852 0.856 0.925 0.881 0.825 0.891 0.825 0.891 0.892 0.89	0.124 2.788 3.657 0.855 3.565 0.757 0.658 0.707 0.665 0.715 0.200 3.657 0.855 3.414 0.707 0.665 0.716 0.200 3.189 3.657 0.855 3.414 0.802 0.716 0.665 0.200 3.189 3.657 0.855 3.414 0.802 0.718 0.200 3.189 3.657 0.855 3.200 0.819 0.7718 0.200 3.270 3.271 0.855 3.200 0.819 0.7718 0.600 0.400 3.271 0.603 0.819 0.7718 0.600 3.427 3.657 0.955 3.201 0.855 0.884 0.7718 0.600 3.427 3.657 0.955 3.000 0.832 0.884 0.950 0.600 0.800 0.		303	00000000000000000000000000000000000000	755 C. 755 C. 855 C. 755 C. 855 C. 755 C. 855 C. 85	1.119 3.660 C.756 C.865 I.119 3.660 C.756 C.865 I.119 3.660 C.756 C.865 I.164 3.660 C.756 C.865 I.164 3.660 C.865 C.861 C.861 I.164 3.860 C.861 I.164 3.860 C.861 I.166 C.861
0.15c 2.824 3.657 0.855 3.576 0.779 0.655 0.2175 2.978 3.657 0.925 3.214 0.925 0.779 0.655 0.250 3.185 3.657 0.925 3.201 0.832 0.779 0.653 0.250 3.276 3.276 0.925 3.201 0.832 0.779 0.655 0.400 3.276 3.657 0.925 3.201 0.832 0.794 0.650 0.400 3.276 3.657 0.925 3.201 0.832 0.794 0.926 0.400 3.512 3.657 0.925 3.012 0.856 0.894 0.926 0.400 3.512 3.657 0.925 3.012 0.856 0.926 0.926 0.920 3.512 3.657 0.925 3.201 0.856 0.926	0.15c 2.824 3.057 0.855 3.576 0.877 0.653 0.200 0.200 3.055 0.657 0.855 3.414 0.692 0.713 0.2200 3.056 3.057 0.855 3.414 0.852 0.714 0.653 0.2200 3.058 3.057 0.855 3.414 0.852 0.714 0.250 3.057 0.855 3.414 0.852 0.714 0.250 3.270 3.271 0.651 0.715 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.640 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.815 0.715 0.81	0	03	0.000000000000000000000000000000000000	6.39	1.124 1.124 1.124 1.124 1.124 1.124 1.124 1.125 1.125 1.125 1.252 1.263 1.273 1.273 1.274 1.273 1.274 1.274 1.274 1.275
0.175 2.9C5 3.C57 C.877 3.485 C.791 0.693 0. 0.200 3.088 3.C57 C.895 3.414 C.802 0.718 0.220 3.189 3.C57 C.954 3.201 0.6832 C.794 0. 0.200 3.189 3.C57 C.954 3.201 0.6832 C.794 0. 0.400 3.189 3.C57 C.954 3.124 0.685 0.718 0.757 0.695 0.490 0.757 0.695 0.490 0.790 0.791 0.685 0.490 0.790 0	0.175 2.9C5 3.C57 C.877 3.485 C.791 0.693 0. 0.200 3.089 3.C57 C.895 3.300 0.832 C.794 0. 0.200 3.089 3.C57 C.895 3.300 0.832 C.794 0. 0.300 3.189 3.C57 C.954 3.124 0.843 0.757 0. 0.300 3.189 3.C57 C.976 3.124 0.843 0.757 0. 0.450 3.327 3.C57 C.976 3.124 0.843 0.757 0. 0.500 3.427 3.C57 C.976 3.124 0.843 0.757 0. 0.500 3.427 3.C57 C.976 3.124 0.843 0.757 0. 0.500 3.427 3.C57 C.975 1.C22 2.979 0.862 0.962 0. 0.500 3.427 3.C57 1.C29 2.079 0.862 0.962 0. 0.500 3.427 3.C57 1.C29 2.079 0.862 0.962 0. 0.500 3.757 2.963 1.C22 2.979 0.962 0.973 0.975 0.900 1.C27 0.000 1.C27 0.C27 0.000 1.C27 0.C27 0.C	;	3	1786.00 0.446.00 0.446.00 0.000.11	575 C.788 C.987 5467 C.788 C.987 566 C.982 C.977 357 C.982 C.977 358 C.982 I.007 578 C.987 I.007 578 C.987 I.007 578 C.987 I.007 578 C.987 I.183 574 C.991 I.257 578 C.991 I.337 578 C.991 I.337 578 C.991 I.337 578 C.991 I.337	1.154 1.164
0.200 2.978 3.657 0.895 3.414 0.6912 0.712 0.625 3.689 3.689 3.657 0.925 3.326 0.893 0.797 0.895 0.995	0.200 2.978 3.C57 0.895 3.414 0.802 0.712 0.725 0.250 3.089 3.C57 0.925 3.212 0.812 0.813 0.757 0.250 3.250 3.275 0.925 3.206 0.813 0.757 0.925 0.400 3.275 3.C57 0.925 3.206 0.812 0.845 0.845 0.950 3.427 3.C57 0.925 3.207 0.862 0.845 0.946 0.950 3.427 3.C57 0.925 3.207 0.862 0.845 0.946 0.950 3.427 3.C57 0.925 2.977 0.862 0.845 0.965 0.940 0.950 3.512 3.C57 0.925 2.977 0.862 0.945 0.950 0.945 0.950 3.512 3.C57 0.925 2.977 0.862 0.965 0.965 0.946 0.973 0.973 0.970 3.551 2.948 1.C52 2.977 0.862 0.992 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.970 0.972 0.972 0.970 0.972	0.1	,	00000000000000000000000000000000000000	2562 C.989 C.9826 C.9828 C.982	1.143 2.574 C.788 C.90C I.164 3.502 C.90C I.165 3.502 C.90C II.165 3.502
0.250 3.689 3.657 0.925 3.306 0.837 0.757 0.956 3.126 0.845 0.624 0.940 3.695 3.657 0.955 3.306 0.837 0.845 0.440 3.657 0.956 3.012 0.845 0.845 0.940 3.427 3.627 0.955 3.012 0.856 0.845 0.950 3.427 3.627 1.022 2.973 0.865 0.865 0.865 0.950 3.427 3.627 1.022 2.973 0.865 0.865 0.965 0.750 3.427 3.627 1.022 2.973 0.865 0.965 0.965 0.750 3.427 3.627 1.022 2.973 0.865 0.965 0.965 0.965 0.973 0.975	0.250 3.689 3.657 0.825 3.201 0.814 0.824 0.757 0.400 3.189 3.657 0.925 3.203 0.835 0.824 0.400 3.127 3.657 0.955 3.203 0.835 0.824 0.400 3.327 3.657 0.955 3.037 0.865 0.865 0.400 3.512 3.627 1.625 3.037 0.856 0.865 0.865 0.600 3.512 3.627 3.625 1.641 2.903 0.856 0.956 0.956 0.900 3.512 3.623 1.641 2.903 0.824 0.936 0.900 3.525 2.955 1.000 3.757 2.955 1.000 2.714 0.894 0.935 0.900 1.000 3.757 2.955 1.000 2.714 0.894 0.935 0.900 1.000 3.757 2.955 1.000 2.714 0.894 0.935 0.900 1.000 3.757 2.955 1.000 2.714 0.894 0.935 0.900 1.000 3.757 2.955 1.000 2.714 0.894 0.935 0.900 1.900	5.0 605.	Š	0.420 0.444 0.044 0.044 0.044 0.044 0.044 0.044	252 C.901 C.947 C.952 C.953 C.954 C.954 C.954 C.954 C.954 C.954 C.955 C.	1.164 3.502 C.9C1 C.92C1 1.164 3.502 C.9C1 C.9C2
C.300 3-189 3-057 C.478 3-124 0.845 0.826 0.405	C.350 3-189 3-C57 C.578 3-124 C.852 C.854 C.550 C.550 3-3174 3-C57 C.578 3-124 C.855 C.864 C.550 C.550 3-517 3-C57 C.578 3-030 C.855 C.864 C.550 3-512 C.851 C.855 C.864 C.550 3-512 C.861 C.590 3-72 C.861 C.590	.926 0.2	0	6.44 6.44 6.44 6.44 6.44 6.44 6.44 6.44	2467 0.0814 0.047 0.087 0.0824 0.0824 0.0834 1.087 0.0847 1.089 0.0847 1.089 0.089 1.265 0.089 1.256 0	1.104 3.467 1.1187 3.368 0.834 1.202 1.203 1.203 1.203 1.203 1.203 1.203 1.204 1.304
C.350 3.270 3.627 C.976 3.012 C.055 C.065 C.066 C.066 3.427 3.045 1.052 2.979 C.862 C.862 C.966 C.950 3.427 3.045 1.052 2.979 C.862 C.862 C.966 C.970 3.427 3.045 1.052 2.979 C.862 C.862 C.966 C.970 3.427 3.045 1.055 2.832 C.861 C.956 C.966 C.966 C.970 3.727 2.956 1.089 2.714 C.966 C.956 C.966 C.970 3.727 2.955 1.089 2.714 C.966 C.975 C.970 1.100 3.872 2.955 1.089 2.714 C.966 C.975 C.970 1.100 3.872 2.969 C.971 C.970 C.971 C.970 C.971 C.970 C.970 C.971 C.970 C.971 C.970 C.971	C.350 3.270 3.627 C.976 3.012 C.055 C.065 C.066 C.060 3.027 3.023 1.024 2.973 C.065 C.066 C.060 3.027 3.023 1.024 2.973 C.065 C.066 C.060 3.020 3.021 2.065 1.002 2.973 C.061 0.956 C.060 0.700 3.727 2.966 1.007 2.714 C.061 0.973 C.060 0.700 3.727 2.966 1.007 2.714 C.061 0.973 C.060 0.700 3.727 2.955 1.008 2.714 C.061 0.973 C.060 1.000 3.727 2.955 1.008 2.714 C.061 0.973 C.061 1.000 3.727 2.955 1.008 2.714 C.061 0.973 C.061 1.000 3.727 2.955 1.008 2.714 C.061 0.973 C.061 1.000 3.727 2.966 1.104 2.514 C.091 1.027 1.027 C.091	036	O	1.053 0.030 0.030 0.030 0.030	356 0.0824 0.0936 0.0834 0.0000 0.0834 0.0000 0.000	1.187 3.358 0.024 (.575 1.202 3.557 0.0324 (.575 1.203 3.213 0.0334 1.005 1.203 3.213 0.0340 1.003 1.306 3.546 0.0857 1.105 1.316 2.046 0.0857 1.105 1.316 2.047 0.037 1.105 1.442 2.719 0.031 1.205 1.442 2.719 0.031 1.205 1.442 2.719 0.031 1.332 1.472 2.719 0.031 1.332
0.400 3.432/ 3.027 0.473 3.036 0.865 0.865 0.500 3.452/ 3.023 1.051 2.979 0.865 0.865 0.665 0.500 3.452/ 3.023 1.051 2.979 0.865 0.865 0.665 0.700 3.452 3.023 1.051 2.979 0.865 0.965 0.700 3.452 2.965 1.001 2.914 0.894 0.935 0.900 3.727 2.935 1.009 2.714 0.894 0.935 0.975 0.9	0.500 3.512/ 3.027 0.473 3.030 0.865 0.865 0.665 0.500 3.512 3.023 1.041 2.993 0.865 0.865 0.865 0.500 3.512 3.023 1.041 2.993 0.865 0.865 0.865 0.500 3.512 3.023 1.041 2.993 0.865 0.865 0.665 0.865	. 544 0.3	ပ	000000000000000000000000000000000000000	257 0.832 1.00C 213 0.842 1.030 213 0.844 1.030 214 0.844 1.034 244 0.844 1.164 247 0.844 1.265 248 0.844 1.265 249 0.844 1.250 249 0.844 1.350 241 1.332 241 0.844 1.332	1.232 3.357 0.882 1.00C 1.243 3.27 3.286 0.8640 1.030 1.243 1.243 3.108 0.8640 1.009 1.263 1.263 0.8640 1.009 1.307 0.864 1.265 1.307 0.864 1.265 1.462 0.864 1.265 1.462 0.864 1.265 1.462 0.864 1.265 1.462 0.864 1.265 1.462 0.864 1.265 1.462 0.864 1.265 1.462 0.864 1.332 1.462 0.463 1.332 1.463 0.463 1.332 1.463 0.463 1.332 1.463 0.463 1.332 1.463 0.463 0.463 1.463 0.46
C.45C 3.427 3.025 1.021 2.973 0.852 0.862 0.500 3.427 3.025 1.021 2.973 0.862 0.875 0.700 3.452 1.025 2.973 0.862 0.975 0.700 3.452 2.985 1.035 2.832 0.881 0.935 0.955 0.975	C.45C 3.427 3.045 1.027 2.979 0.862 0.662 0.500 3.427 3.045 1.041 2.979 0.862 0.662 0.700 3.659 2.966 1.070 2.714 0.894 0.936 0.975 0.700 3.659 2.966 1.070 2.714 0.894 0.936 0.936 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937 0.937 0.930 0.937	150	0	0.00.1	2.86 0.840 1.030 0.040 0.080 0.0847 1.053 0.040 0.087 1.132 0.040 0.087 1.132 0.087 1.250 0.087 1.250 0.087 1.250 0.087 1.332 0.087 1.332 0.087 1.332 0.087 1.332 0.087 1.332 0.097 1.332	1.227 2.286 C.845 1.035 1.243 3.619 C.845 1.053 1.243 3.619 C.845 1.009 1.345 2.046 C.865 1.165 1.345
0.500 3.427 3.049 1.001 2.903 0.800 0.500 3.427 3.049 1.001 2.903 0.803 0.803 0.803 1.001 2.903 1.001 2.903 0.803 0.803 1.001 3.503 1.002 3.714 0.804 0.905	0.500 3.427 3.045 1.002 2.777 0.002 0.003	9.0	\circ	650*1	213 C.847 1.053 246 C.854 1.049 504 C.864 1.182 705 C.864 1.255 707 C.891 1.255 708 C.891 1.384 547 C.911 1.382 547 C.911 1.384	1.243 3.213 C.847 1.053 1.246 3.148 C.857 1.0040 1.306 3.046 C.857 1.1020 1.307 2.46 C.857 1.1020 1.307 2.703 C.807 1.206 1.442 2.719 C.807 1.206 1.457 2.719 C.807 1.306 1.337 1.457 2.719 C.807 1.337 1.337 1.457 2.719 C.807 1.337 1.337 1.447 2.719 C.807 1.337 1.447 2.719 C.807 1.337 1.44
0.500 3.512 3.623 1.031 2.903 0.903 0.903 0.700 3.591 2.905 1.000 2.714 0.000 0.903	0.500 3.512 3.623 1.031 2.932 0.932 0.936 0.930 0.3503 3.757 2.985 1.089 2.714 0.884 0.935 0.936 0.936 0.936 0.937 0.936 0.937 2.985 1.089 2.714 0.884 0.937 0.936 0.936 0.937 2.953 1.100 3.757 2.953 1.100 2.945 0.900 0.937 0.936 1.200 4.027 0.936 0.937 1.000 3.757 2.959 1.134 2.954 0.917 1.027 0.936 1.200 4.027 0.912 1.200 4.257 2.898 1.225 2.366 0.917 1.027 0.917 1.000 4.487 2.898 1.285 2.367 0.938 1.285 0.936 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.287 1.288 1.287 1.288 1.287	. o	•	650.1	.108 0.859 1.099 .546 0.867 1.132 .971 0.867 1.265 .793 0.891 1.256 .719 0.897 1.294 .547 0.911 1.332	1.240 3.108 0.859 1.099 1.306 3.546 0.867 1.132 1.346 7.977 1.132 1.35 7.743 0.891 1.265 1.442 2.719 0.897 1.294 1.442 2.719 0.897 1.294 1.472 2.719 0.911 1.332
0.700 3.591 2.989 1.030 2.711 0.891 0.995 0.900 3.752 2.959 1.000 2.714 0.894 0.995 0.995 0.995 0.995 0.995 0.995 0.995 0.995 1.000 3.872 2.959 1.108 2.645 0.900 0.999 0.995 1.100 3.872 2.959 1.108 2.645 0.900 0.999 0.995 1.200 4.112 2.898 1.255 2.356 0.912 1.055 0.912 1.600 4.415 2.898 1.255 2.356 0.922 1.155 0.125 0.996 1.200 4.415 2.898 1.255 2.356 0.936 1.256 0.957 1.256 0.996 1.200 4.415 2.898 1.328 2.123 0.948 1.256 0.997 1.250 0.997 1.250 0.998 1.200 4.415 2.898 1.437 2.017 0.948 1.402 1.250 2.200 4.415 2.898 1.437 2.017 0.959 1.433 1.250 0.959 1.433 1.250 0.959 1.433 1.250 0.959 1.433 1.250 0.959 1.433 1.250 0.959 1.433 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.651 1.250 0.959 1.652 1.250 0.959 1.651 1.250 0.959	0.700 3.591 2.985 1.030 2.714 0.886 0.935 0.900 3.725 2.955 1.000 2.714 0.894 0.975 0.975 0.900 3.725 2.955 1.000 2.714 0.894 0.975	836	\circ		977 C.887 1.185 G.887 1.185 G.884 1.205 G.891 1.205 G.891 1.206 G.897 1.326 G.897 1.326 G.897 1.332 G.897 1.332 G.918 G.918 1.332 G.918 1.332 G.918 1.332 G.918 1.332 G.918 G.918 1.332 G.918 G.	1.300 3.046 0.807 1.152 1.32 1.32 1.32 1.32 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30
C.800 3.659 2.566 1.010 2.111 0.895 0.995 0.990 3.122 2.955 1.108 2.014 0.895 0.995	C.800 3.659 2.566 1.010 2.774 0.895 0.995 0.997	. 974 0.7	12	1.132	.977	1,346 2,977 0,875 1,165 1,165 1,367 1,367 2,467 0,864 1,256 1,442 2,719 0,897 1,294 1,472 2,415 2,411 1,384 1,542 2,471 0,911 1,384 1,542 2,471 0,911 1,384
C.900 3.722 2.952 1.108 2.945 C.900 C.900 1.100 3.757 2.952 1.108 2.519 C.900 C.900 C.900 1.100 3.757 2.952 1.108 2.519 C.900 C.900 1.000 3.612 2.953 2.959 1.102 2.504 C.912 1.000 C.912 1.000 4.112 2.898 1.225 2.356 C.922 1.125 0.125 1.200 4.257 2.898 1.225 2.356 C.930 1.200 0.917 1.000 4.487 2.898 1.255 2.100 C.930 1.200 0.950 1.200 2.100 4.487 2.898 1.400 2.017 C.930 1.200 0.950 1.200 4.487 2.898 1.400 2.017 C.930 1.200 0.950 1.200 4.910 2.898 1.400 2.017 C.944 1.337 1.200 4.910 2.898 1.479 1.959 0.959 1.200 0.950 1.437 1.200 4.910 2.864 1.974 1.979 1.989 0.950 1.437 1.200 4.910 2.864 1.672 1.979 0.950 1.437 1.200 4.910 2.864 1.672 1.700 0.950 1.673 1.520 1.200 4.910 2.864 1.671 1.700 0.965 1.607 1.513 1.200 4.910 2.864 1.671 1.700 0.965 1.651 1.562 1.200 4.910 2.864 1.671 1.700 0.965 1.662 1.651 1.200 4.900 2.918 1.711 1.647 0.965 1.651 1.651 1.662 1.200 4.900 2.755 1.720 0.965 1.661 1.651 1.671 1.671 1.671 1.672 1.673 1.675	C.900 3.722 2.932 1.104 2.945 0.903 0.903 1.100 3.722 2.932 1.104 2.514 0.903 0.903 1.100 3.913 2.953 1.104 2.514 0.903 0.903 1.005 1.203 2.953 1.104 2.514 0.903 1.005 1.203 2.954 0.917 1.005 1.203 1.203 2.354 0.917 1.005 1.203 1.203 2.354 0.917 1.005 0.903 1.20	3.0	•	1.165	261 C.884 1.2C9 C.894 1.2C9 C.894 1.2C9 C.894 1.2C9 C.864 1.322 C.564 1.332 C.	1,307 2,467 C.864 1,2CG 1,404 2,743 C.8941 1,25C 1,442 2,719 C.8847 1,204 1,472 2,674 C.411 1,384 1,55C 1,55C 1,541 1,384 1,55C 1,55C 1,541 1,384 1,55C 1,55
1.000 3.679 2.992 1.104 2.995 0.912 1.000 3.679 2.992 1.105 2.904 0.917 1.005 0.912 1.200 4.112 2.908 1.104 2.904 0.917 1.005 0.912 1.005 0.912 1.005 0.912 1.200 4.112 2.898 1.225 2.366 0.917 1.005 0.917 1.005 0.917 1.005 0.918 1.200 4.497 2.898 1.200 2.247 0.936 1.200 1.200 0.918 1.200 0.918 1.200 0.918 1.200 0.918 1.200 0.918 1.200 0.918 1.200 0.918 1.200 0.920 0.920 1.200 0.920 1.200	1.000 3.672 2.922 1.134 2.934 0.912 1.027 0.925 1.120 3.672 2.929 1.134 2.934 0.917 1.027 0.925 1.129 2.939 1.125 2.949 1.125 2.949 0.917 1.055 0.912 1.900 4.257 2.898 1.255 2.345 0.936 1.240 0.917 1.055 0.925 1.129 0.939 1.200 4.487 2.898 1.328 2.123 0.938 1.240 0.941 1.240 0.925 1.129 0.939 1.900 4.487 2.898 1.437 2.017 0.939 1.240 0.925 1.1357 1.220 4.910 2.898 1.437 2.017 0.944 1.357 1.280 0.944 1.357 1.280 0.959 1.402 1.280 0.959 1.402 1.280 0.959 1.402 1.280 0.959 1.402 1.280 0.959 1.402 1.280 0.959 1.503 1.402 1.280 0.959 1.503 1.402 1.280 0.959 1.503 1.402 1.280 0.959 1.503 1.402 1.280 0.959 1.503 1.673 1.280 0.959 1.503 1.673 1.280 0.959 1.503 1.673 1.280 0.959 1.503 1.673 1.280 0.959 1.503 1.673 1.280 0.959 1.503 1.625 1.280 0.959 1.503 1.625 1.280 0.959 1.201 1.201 1.201 1.201 0.965 1.662 1.262 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 1.201 0.967 0.967 1.201 0.967	200	9	1.205	743 C.841 1.25C C. 743 C.847 1.244 C. 847 1.384 C. 411 1.384 C. 411 1.384 C. 411 1.384 C. 411 C. 412 C. 413	1.442 2.743 6.891 1.256 6.1442 2.719 6.897 1.294 6.1442 2.719 6.897 1.294 6.1432 6.1412 1.432 6.1412 1.432 6.1412 1.432 6.1412 1.432 6.1412 1.432
1.200	1.200	987	٠,	1.250	715 C.847 1.248 C.548 C.548 C.548 C.548 1.332 C.548 1.386 C.548 C.	1.442 2.419 C.844 1.432 C.444 1.442 2.454 2.454 2.454 1.433 C.411 1.434 2.454
1.500 4.029 2.909 1.225 2.366 0.917 1.095 1.500 4.122 2.898 1.225 2.369 0.917 1.095 1.225 1.125 1.125 1.126 0.917 1.000 4.125 2.898 1.226 2.369 0.938 1.226 1.226 1.125 1.000 4.415 2.898 1.328 2.123 0.938 1.226 0.938 1.328 2.123 0.938 1.226 0.938 1.328 2.100 4.415 2.898 1.400 2.017 0.944 1.317 1.226 2.200 4.319 2.898 1.400 2.017 0.948 1.402 1.226 2.200 4.319 2.886 1.479 1.989 0.948 1.402 1.226 2.200 4.316 2.898 1.479 1.989 0.948 1.402 1.226 2.200 4.316 2.886 1.479 1.989 0.959 1.473 1.226 2.200 4.316 2.864 1.672 1.970 0.953 1.473 1.226 2.200 4.316 2.864 1.652 1.652 1.700 0.953 1.673 1.226 1.652 1.226 2.800 1.691 1.671	1.500 4.029 2.909 1.194 2.436 0.917 1.095 1.400 4.112 2.898 1.225 2.366 0.922 1.125 1.200 4.257 2.898 1.225 2.347 0.922 1.125 1.800 4.487 2.898 1.390 2.847 0.939 1.200 1.900 4.487 2.898 1.365 2.123 0.938 1.280 1.900 4.487 2.898 1.497 2.017 0.944 1.387 1.200 4.967 2.898 1.497 2.017 0.944 1.387 1.2200 4.783 2.898 1.497 2.017 0.944 1.387 1.2200 4.783 2.898 1.479 1.999 0.948 1.402 1.200 2.200 4.783 2.898 1.479 1.999 0.948 1.402 1.200 2.200 4.910 2.896 1.479 1.999 0.948 1.402 1.200 2.300 4.910 2.804 1.574 1.827 0.953 1.473 1.250 2.900 4.910 2.804 1.602 1.702 0.965 1.558 1.503 1.200 2.800 2.818 1.701 1.677 0.965 1.607 1.558 1.200 3.000 2.818 1.701 1.647 0.965 1.607 1.607 1.200 2.200 2.795 1.720 0.965 1.607 1.607 1.200 2.800 2.795 1.720 1.607 1.607 1.607 1.200 2.800 2.795 1.720 1.607 1.607 1.607 1.200 2.800 1.720 1.607 1.60		つ ′-	7 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 547	
1.500 4.112 2.898 1.255 2.366 C.922 1.125 0.1150 4.287 2.898 1.285 2.369 C.926 1.163 0.1163 0.1160 4.287 2.898 1.280 2.247 C.930 1.260 1.260 4.415 2.898 1.328 2.183 0.938 1.280 1.900 4.415 2.898 1.300 2.075 0.938 1.280 0.938 1.280 2.000 4.415 2.898 1.400 2.075 0.941 1.317 1.280 2.100 4.644 2.898 1.400 2.077 0.944 1.387 1.280 2.200 4.719 2.898 1.479 1.959 0.948 1.402 1.280 2.200 4.719 2.886 1.479 1.959 0.959 1.402 1.280 2.200 4.910 2.886 1.512 1.909 0.959 1.402 1.280 2.200 4.910 2.864 1.512 1.909 0.959 1.593 1.502 1.280 2.200 4.910 2.864 1.602 1.700 0.959 1.593 1.503 1.280 2.200 5.013 2.852 1.652 1.700 0.959 1.653 1.653 1.280 2.200 5.140 2.818 1.711 1.647 0.965 1.651 1.655 1.200 5.110 2.818 1.711 1.647 0.965 1.651 1.651 1.200 5.110 2.818 1.711 1.647 0.965 1.651 1.651 1.200 5.110 2.718 1.711 1.647 0.965 1.651 1.6	1.600 4.112 2.898 1.225 2.366 C.922 1.125 0.163 0.460 4.257 2.898 1.225 2.369 C.926 1.163 0.1260 4.339 2.898 1.226 2.124 C.930 1.226 0.1260 4.415 2.898 1.328 2.123 0.938 1.226 0.1260 4.467 2.898 1.368 2.123 0.948 1.226 0.926 1.300 4.467 2.898 1.497 2.017 C.944 1.387 1.226 2.20 4.319 2.898 1.497 2.017 C.944 1.387 1.226 2.300 4.319 2.898 1.497 2.017 C.944 1.387 1.226 2.300 4.319 2.886 1.497 2.017 C.946 1.387 1.226 2.300 4.910 2.864 1.574 1.827 0.959 1.402 1.226 2.300 4.910 2.864 1.672 1.727 0.959 1.437 1.258 1.226 2.300 4.910 2.864 1.672 1.727 0.959 1.673 1.258 1.300 2.800 2.818 1.711 1.671 C.963 1.625 1.627 1.328 2.300 2.289 1.728 1.301 1.67	300	-	756.1	471 C.910 1.432	2 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
1.500 4.182 2.898 1.255 2.309 0.926 1.163 0. 1.600 4.257 2.898 1.290 2.247 0.930 1.200 1.200 1.900 4.415 2.898 1.328 2.103 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.280 0.938 1.387 1.980 0.959 1.357 1.980 0.959 1.982 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.959 1.980 1.980 0.950 1.980 1.980 0.950 1.980 1.980 0.950 1.980 1.9	1.500 4.182 2.898 1.255 2.309 0.926 1.163 0.1600 4.257 2.898 1.290 2.247 0.930 1.200 1.200 1.200 4.339 2.898 1.328 2.182 0.938 1.200 1.200 4.415 2.898 1.300 2.012 0.938 1.200 1.900 4.487 2.898 1.400 2.017 0.941 1.317 1.200 2.010 4.644 2.898 1.400 2.017 0.941 1.317 1.200 4.316 2.898 1.479 1.999 0.959 1.402 1.200 2.300 4.847 2.898 1.479 1.999 0.959 1.402 1.200 2.300 4.910 2.804 1.512 1.909 0.959 1.402 1.200 2.900 4.910 2.804 1.602 1.700 0.959 1.437 1.200 2.900 4.910 2.804 1.602 1.700 0.959 1.633 1.200 2.800 2.900 1.700 0.959 1.558 1.500 2.900 2.100 2.800 1.601 1.700 0.960 1.601 1.501 1.200 2.800 1.701 1.671 0.964 1.601 1.501 1.200 2.800 2.800 1.701 1.671 0.964 1.601 1.200 2.800 2.700 2.800 1.701 1.671 0.964 1.601 1.200 2.800 1.701 1.671 0.964 1.601 1.200 2.800 1.701 1.671 0.964 1.601 1.200 2.800 1.701 1.671 0.964 1.601 1.200 2.800 1.701 1.671 0.964 1.601 1.601 1.200 2.800 1.701 1.671 0.964 1.601 1.601 1.200 2.800 1.200 1.200 1.601 1.601 1.200 2.800 1.200 1.601 1.601 1.200 2.800 1.200 1.200 1.601 1.601 1.200 1.200 1.200 1.601 1.601 1.200 2.800 1.200 1.601 1.601 1.200 2.800 1.200 1.200 1.601 1.601 1.200 2.800 1.200 1.601 1.601 1.200 2.800 1.200 1.601 1.601 1.200 2.800 1.200 1.200 1.601 1.601 1.200	0.0	,	1.432		
1.600 4.257 2.898 1.290 2.247 C.930 1.2CC 0.1.70C 4.339 2.898 1.328 2.182 C.934 1.241 0.1.70C 4.415 2.898 1.328 2.182 C.934 1.241 0.1.900 4.415 2.898 1.407 2.017 C.941 1.317 1.280 2.200 4.562 2.898 1.407 2.017 C.944 1.317 1.280 2.200 4.719 2.898 1.479 1.959 0.948 1.402 1.280 2.200 4.719 2.898 1.479 1.959 0.959 1.402 1.280 2.30C 4.910 2.886 1.512 1.909 0.953 1.473 1.2.200 4.910 2.886 1.574 1.827 0.953 1.473 1.2.200 4.910 2.864 1.674 1.876 0.955 1.503 1.503 1.2.200 2.280C 1.652 1.652 1.700 0.965 1.653 1.657 1.227 0.961 1.566 1.227 0.962 1.657 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.668 1.201 0.965 1.667 1.201 0.965 1.667 1.201 0.965 1.668 1.201 0.965 1.667 1.201 0.965 1.201 0.201 0.201 0.201 0.201 0.965 1.201 0.201	1.600 4.257 2.898 1.290 2.247 C.930 1.2CC 0.1.70C 4.39 2.898 1.328 2.182 C.934 1.241 0.1.800 4.415 2.898 1.365 2.182 C.934 1.241 0.1.800 4.487 2.898 1.407 2.017 C.944 1.317 1.280 2.100 4.562 2.898 1.407 2.017 C.944 1.317 1.280 2.200 4.564 2.898 1.407 2.017 C.944 1.317 1.280 2.200 4.763 2.896 1.479 1.959 0.959 1.402 1.357 1.2.200 4.763 2.886 1.946 1.950 0.959 0.959 1.402 1.2.200 4.910 2.864 1.946 1.827 0.959 1.473 1.2.200 4.910 2.864 1.602 1.878 0.959 1.473 1.2.200 4.910 2.864 1.602 1.727 0.961 1.558 1.200 2.800 2.852 1.652 1.727 0.961 1.558 1.625 1.200 3.100 2.867 1.720 1.677 0.964 1.651 1.561 1.370 0.964 1.651 1.651 1.370 0.964 1.651 1.651 1.370 0.964 1.651 1.651 1.370 0.964 1.651 1.651 1.200 3.209 2.755 1.726 1.617 0.965 1.651 1.651 1.200 3.209 2.755 1.726 1.617 0.965 1.651 1.675 1.300 3.209 2.775 1.726 1.617 0.965 1.651 1.675 1.300 3.209 2.775 1.726 1.617 0.967 1.675 1.275 1.675 1.275 1.675 1.675 1.275 1.275 1.677 0.967 1.675 1.275 1.275 1.671 0.967 1.675 1.275 1.275 1.275 1.275 1.671 0.967 1.675 1.275 1.275 1.275 1.275 1.275 1.275 1.275 1.275 1.275 1.275 1.275 1.2784 1.775 1.677 0.967 1.675 1.27	255	,	1 9 9 1	14.4	
1.70c 4.339 2.898 1.328 2.182 C.534 1.241 O. 1.800 4.415 2.898 1.365 2.123 0.938 1.280 O. 1.800 4.487 2.898 1.365 2.123 0.938 1.280 O. 1.900 4.487 2.898 1.490 2.017 C.944 1.337 1.280 O. 2.100 4.564 2.898 1.479 1.959 0.964 1.437 1.337 1.250 4.719 2.806 1.512 1.909 0.959 1.402 1.250 0.950 1.437 1.250 0.950 1.437 1.250 0.950 1.437 1.250 0.950 1.437 1.250 0.950 1.437 1.250 0.950 1.258 1.250 0.950 1.285 1.287 1.287 1.287 0.965 1.687 1.285 1.287 1.287 0.965 1.687 1.285 1.287 1.287 0.965 1.687 1.285 1.287 1.287 1.287 0.965 1.688 1.285 1.285 1.287 1.287 1.287 0.965 1.688 1.285 1.285 1.287 1.287 1.287 0.965 1.288 1.285 1.287 1.287 1.287 0.965 1.288 1.285 1.287 1.287 1.287 0.965 1.288 1.285 1.287 1.287 1.287 0.965 1.288 1.287 1.287 1.287 0.965 1.288 1.288 1.288 1.288 1.288 1.288 1.288 1.288 1.288 1.288 1.281 1.2888 1.288 1.288 1.288 1.2888 1.288 1.288 1.2888 1.2	1.70c 4.339 2.898 1.328 2.182 C.534 1.241 O. 1.800 4.415 2.898 1.365 2.162 0.938 1.280 O. 1.800 4.487 2.898 1.365 2.172 0.941 1.317 1.800 4.562 2.898 1.457 2.017 C.944 1.337 1.337 1.200 4.564 2.898 1.457 2.017 C.944 1.337 1.337 1.2200 4.789 2.886 1.479 1.999 0.950 1.437 1.327 2.300 4.910 2.886 1.512 1.909 0.959 1.432 1.250 4.910 2.864 1.602 1.788 0.953 1.473 1.250 0.950 1.533 1.200 4.910 2.864 1.602 1.788 0.957 1.533 1.200 2.800 2.613 2.864 1.602 1.700 0.965 1.558 1.258 1.200 2.800 2.852 1.652 1.700 0.965 1.657 1.568 1.200 2.800 2.800 1.701 1.671 0.965 1.657 1.651 1.300 2.180 2.807 1.720 1.631 0.965 1.651 1.300 2.209 2.795 1.720 1.631 0.965 1.651 1.300 2.209 2.795 1.720 1.611 0.965 1.651 1.200 2.209 2.795 1.720 1.611 0.965 1.651 1.651 1.200 2.209 2.795 1.720 1.611 0.965 1.651 1.651 1.200 2.209 2.795 1.720 1.611 0.965 1.651 1.612 1.200 2.209 2.795 1.720 1.611 0.967 1.615 1.200 2.209 2.795 1.720 1.611 0.967 1.615 1.200 2.200 2.795 1.720 1.611 0.967 1.615 1.200 2.200 2.795 1.720 1.611 0.967 1.615 1.200 2.200 2.795 1.790 1.611 0.967 1.615 1.200 2.200 2.795 1.790 1.611 0.967 1.615 1.200 2.200 2.795 1.790 1.611 0.967 1.615 1.200 2.200 2.795 1.790 1.611 0.967 1.615 1.200 2.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.611 0.967 1.615 1.200 2.795 1.790 1.200 2.795 1.790 1.200 2.795 1.790 1.200 2.795 1.790 1.200 2.795 1.790 1.200 2.795 1.790 1.200 2.795	9-1 856	_	1.536	248 0.427 1.536	1.54.5 C.54.5 C.54.5 L.53.5 L.
1.800 4.415 2.898 1.365 2.123 0.938 1.280 0.2 1.900 4.487 2.898 1.400 2.070 0.941 1.317 1.2 1.000 4.487 2.898 1.400 2.070 0.941 1.317 1.2 1.000 4.562 2.898 1.400 2.070 0.944 1.337 1.3 1.2 1.000 4.544 2.898 1.400 2.017 0.944 1.357 1.3 1.2 1.000 0.959 1.437 1.3 1.2 1.000 0.959 1.437 1.2 1.909 0.959 1.437 1.2 1.909 0.959 1.437 1.2 1.900 0.959 1.437 1.2 1.900 0.959 1.437 1.2 1.900 0.959 1.437 1.2 1.900 0.959 1.558 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	1.800 4.415 2.898 1.365 2.123 0.938 1.280 0.2 1.900 4.487 2.898 1.400 2.070 0.941 1.317 1.2 2.000 4.562 2.898 1.407 2.017 0.941 1.317 1.2 2.100 4.562 2.898 1.407 2.017 0.944 1.357 1.357 1.2 2.200 4.716 2.898 1.473 1.959 0.959 1.402 1.2 2.200 4.716 2.898 1.473 1.909 0.959 1.402 1.2 2.200 4.910 2.898 1.974 1.827 0.953 1.473 1.2 2.900 4.910 2.864 1.602 1.788 0.959 1.533 1.473 1.2 2.900 4.910 2.864 1.602 1.727 0.962 1.558 1.593 1.2 2.900 5.013 2.892 1.602 1.700 0.962 1.607 1.2 2.900 5.100 2.830 1.671 1.700 0.962 1.607 1.2 2.900 5.100 2.818 1.711 1.700 0.964 1.641 1.3 2.900 5.209 2.795 1.726 1.617 0.966 1.662 1.3 2.900 5.795 1.726 1.617 0.966 1.662 1.3 2.900 5.795 1.726 1.617 0.966 1.662 1.2 3.900 5.209 2.795 1.726 1.617 0.966 1.662 1.2 3.900 5.243 2.784 1.731 1.602 0.967 1.675 1.675 1.875 1.786 1.787 1.675 1.675 1.675 1.675 1.788 1.781 1.602 0.967 1.675 1.875 1.781 1.602 0.967 1.675 1.781 1.781 1.602 0.967 1.675 1.875 1.781 1.781 1.602 0.967 1.675 1.875 1.781 1.781 1.602 0.967 1.675 1.875 1.875 1.781 1.875 1.	000		1.585	253 (253) (2585)	2007 (2007) (2007)
1.900 4.487 2.898 1.400 2.07C C.941 1.317 1.200 4.562 2.898 1.437 2.017 C.944 1.357 1.2.200 4.2164 2.898 1.479 1.959 0.944 1.357 1.2.200 4.719 2.898 1.479 1.999 0.948 1.402 1.999 0.959 1.402 1.200 4.719 2.886 1.946 1.946 1.969 0.959 1.473 1.2.200 4.910 2.864 1.602 1.788 C.957 1.533 1.473 1.2.200 4.910 2.864 1.602 1.788 C.957 1.533 1.2.200 5.013 2.864 1.602 1.727 0.959 1.558 1.2.200 5.013 2.864 1.651 1.671 1.671 1.677 0.969 1.653 1.627 1.2.200 5.160 2.818 1.701 1.677 0.969 1.657 1.657 1.200 5.160 2.818 1.711 1.647 0.969 1.651 1.651 1.200 5.160 5.167 1.720 1.631 C.966 1.668 1.200 5.200 2.755 1.720 1.619 C.966 1.668 1.651 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.607 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.200 5.212 2.755 1.720 1.619 0.967 1.615 1.615 1.615 1.200 5.212 2.755 1.720 1.610 5.200 5.212 2.755 1.720 1.610 5.200 5.212 2.755 1.720 5.200 5.212 1.612 1.200 5.212 5.212 5.755 1.720 5.212 5.2	1.900 4.487 2.898 1.400 2.07C C.941 1.317 1.22.00 4.562 2.898 1.437 2.017 C.944 1.357 1.2.200 4.716 2.898 1.437 2.017 C.944 1.357 1.2.200 4.716 2.898 1.479 1.959 0.968 1.437 1.479 1.959 0.968 1.437 1.2.200 4.716 2.886 1.946 1.867 0.953 1.473 1.2.200 4.910 2.864 1.874 1.827 0.953 1.473 1.220 2.900 4.910 2.864 1.802 1.788 0.957 1.533 1.2.800 2.800 1.602 1.788 0.957 1.558 1.558 1.2.200 2.800 1.607 1.700 0.962 1.558 1.558 1.2.200 2.830 1.671 1.700 0.962 1.607 1.258 1.200 2.830 1.701 1.677 0.963 1.625 1.871 1.700 0.965 1.667 1.671 1.300 2.209 2.785 1.720 1.617 0.965 1.658 1.300 2.209 2.785 1.720 1.617 0.965 1.668 1.300 2.243 2.784 1.720 1.617 0.967 1.675 1.300 2.243 2.784 1.720 1.617 0.967 1.675 1.300 2.243 2.784 1.731 1.602 0.967 1.675 1.875 1.	000		1.031	1631 (2.637	1,747 7,153 0,437 1,631
2.000 4.562 2.898 1.437 2.017 0.944 1.357 1.000 4.564 2.898 1.479 1.959 0.958 1.402 1.200 4.719 2.808 1.479 1.959 0.959 0.958 1.402 1.200 4.719 2.808 1.874 1.812 0.959 0.959 1.473 1.200 4.910 2.864 1.602 1.788 0.953 1.473 1.200 2.800 4.910 2.864 1.602 1.788 0.957 1.533 1.200 2.800 4.910 2.864 1.602 1.700 0.959 1.558 1.200 2.800 2.864 1.601 1.700 0.962 1.558 1.200 2.800 2.818 1.701 1.677 0.962 1.607 1.607 1.200 2.818 1.701 1.677 0.965 1.607 1.200 2.818 1.701 1.677 0.965 1.651 1.671 1.677 0.965 1.651 1.200 2.818 1.711 1.647 0.965 1.651 1.651 1.200 2.800 2.755 1.720 1.619 0.965 1.651 1.619 1.700 0.965 1.668	2.000 4.562 2.898 1.437 2.017 6.944 1.357 1.5 2.210 4.644 2.898 1.479 1.959 0.548 1.402 1.5 2.220 4.789 2.886 1.512 1.909 0.953 1.402 1.5 2.300 4.847 2.875 1.574 1.867 0.953 1.473 1.5 2.500 4.910 2.864 1.602 1.762 0.957 1.533 1.575 1.503 1.575 1.503 1.576 1.503 1.576 1.503 1.576 1.503 1.576 1.503 1.576 1.503 1.576 1.	.000		1.686	1.68C	1.167 2.058 0.940 1.680
2.100 4.644 2.898 1.479 1.939 0.948 1.402 1.200 4.719 2.886 1.512 1.909 0.950 1.437 1.202 2.300 4.719 2.886 1.512 1.909 0.959 1.437 1.200 0.959 1.437 1.200 0.959 1.500 1.437 1.200 0.959 1.500 1.437 1.200 0.959 1.500 1.200 0.959 1.500 1.200 0.959 1.500 1.200 0.959 1.500 1.200 0.959 1.500 1.200 0.959 1.558 1.200 0.959 1.500 1.200	2.103 4.644 2.898 1.479 1.939 0.958 1.902 2.203 4.719 2.886 1.962 1.909 0.953 1.437 1.939 0.959 1.437 1.939 0.959 1.437 1.939 0.959 1.437 1.937 0.959 1.437 1.937 0.959 1.437 1.937 0.959 1.437 1.937 0.959 1.933 1.936 0.959 1.938 0.959 1.938 1.938 0.959 1.938 1.932 0.959 1.958	.600 2-0		1.731	.053 0.942 1.731	1.820 2.053 0.542 1.731
2.300 4.719 2.886 1.512 1.895 0.953 1.473 1.526 1.500 4.910 2.886 1.546 1.827 0.953 1.473 1.526 2.500 4.910 2.884 1.562 1.788 0.957 1.533 1.5280 2.500 4.910 2.884 1.602 1.788 0.957 1.533 1.5280 2.600 4.554 1.652 1.652 1.727 0.951 1.558 1.558 1.5280 2.800 5.012 2.884 1.671 1.700 0.952 1.657 1.657 1.558 1.520 5.000 5.180 2.818 1.701 1.671 0.962 1.657 1.558 1.520 5.180 2.818 1.711 1.647 0.965 1.657 1.657 1.558 1.657 1.558 1.657 1.6	2.3C2 4.7E3 2.8B6 1.512 1.9U3 0.953 1.473 1.526 1.9C3 4.9E3 2.8B6 1.956 1.8E3 0.9553 1.473 1.526 1.9E3 0.9553 1.673 1.526 1.9E3 0.9553 1.9E3 1.9E3 0.9E3 1.9E3 1.9	.000		1.759	.987 C.946 1.759	1.454 1.987 6.946 1.759
2.500 4.847 2.675 1.574 1.627 0.955 1.503 1.2560 4.910 2.864 1.602 1.786 0.957 1.533 1.2500 4.910 2.864 1.602 1.786 0.957 1.533 1.2500 4.955 2.865 1.652 1.727 0.951 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.558 1.258 0.957 1.551 1.259 0.957 1.551 1.259 0.957 1.551 1.259 0.957 1.551 1.259 0.957 1.551 1.251 0.957 1.551 1.259 0.957 1.551 1.259 0.957 1.551 1.259 0.957 1.551 1.259 0.957 1.551 1.551 0.957 1.5	2.500 4.847 2.675 1.574 1.627 0.955 1.503 1.2500 4.910 2.864 1.602 1.788 0.957 1.533 1.2500 4.910 2.864 1.602 1.788 0.957 1.533 1.2500 4.910 2.864 1.602 1.762 0.959 1.558 1.558 1.2500 5.013 2.852 1.652 1.727 0.961 1.558 1.2500 5.00 2.818 1.671 1.700 0.962 1.607 1.558 1.2500 5.167 2.807 1.637 1.657 0.965 1.657 1.556 1.507 1.657 0.965 1.651 1.657 0.965 1.657 0.965 0	2000		1.796	.95C C.94H I.796	1.844 1.950 0.948 1.706
2.500 4.910 2.864 1.602 1.788 0.957 1.533 1.2500 4.910 2.864 1.602 1.762 0.959 1.558 1.558 2.600 5.013 2.852 1.652 1.702 0.959 1.558 1.558 1.200 5.013 2.852 1.651 1.700 0.962 1.607 1.558 1.200 5.140 2.816 1.611 1.647 0.965 1.607 1.555 1.500 5.160 2.818 1.711 1.647 0.965 1.651 1.551 1.651	2.500 4.910 2.864 1.602 1.788 C.957 1.533 1. 2.600 4.954 2.864 1.602 1.762 0.959 1.558 1. 2.800 5.013 2.852 1.652 1.727 0.961 1.556 1. 2.800 5.001 2.841 1.671 1.700 0.962 1.607 1. 2.900 5.102 2.836 1.701 1.657 0.962 1.607 1. 3.000 5.187 2.818 1.711 1.657 0.964 1.647 1.651 1. 3.200 5.187 2.867 1.720 1.619 0.966 1.668 1. 3.400 5.212 2.784 1.732 1.607 0.967 1.615 1. 3.500 5.243 2.773 1.731 1.602 0.967 1.675 1.	2000		2 P - 1	758-1 C-5-2 1-83C	368*1 (35°) /15°1 /25°1
2.600 4.954 2.864 1.626 1.762 0.959 1.558 1. 2.800 5.013 2.852 1.652 1.727 0.961 1.566 1. 2.800 5.102 2.836 1.671 1.700 0.962 1.607 1. 2.900 5.140 2.818 1.701 1.657 0.964 1.657 1. 3.100 5.160 2.818 1.711 1.667 0.964 1.651 1. 3.200 5.167 2.867 1.720 1.631 0.966 1.668 1. 3.800 9.209 2.755 1.726 1.619 0.967 1.655 1.	2.600 4.954 2.864 1.626 1.762 0.959 1.558 1. 2.800 5.013 2.852 1.652 1.727 0.961 1.566 1. 2.800 5.001 2.841 1.671 1.700 0.962 1.607 1. 2.900 5.102 2.830 1.697 1.677 0.962 1.607 1. 3.000 5.140 2.818 1.701 1.657 0.965 1.641 1. 3.200 5.187 2.807 1.720 1.631 0.965 1.651 1. 3.200 5.209 2.755 1.726 1.619 0.966 1.668 1. 3.400 5.212 2.784 1.732 1.607 0.967 1.675 1.	2000	-	ر مورور مورور		
2.700 5.013 2.852 1.652 1.727 0.961 1.566 1.2.800 5.013 2.852 1.651 1.700 0.962 1.607 1.2.800 5.102 2.836 1.671 1.700 0.962 1.607 1.607 1.607 0.963 1.607 1.607 0.964 1.607 1.607 0.965 1.607 1.200 5.167 2.807 1.720 1.631 0.966 1.662 1.3.300 5.209 2.765 1.726 1.619 0.967 1.662 1.663 1.607 0.967 1.607 0.967 1.607 1.607 1.607 0.967 1.607	2.700 5.013 2.852 1.652 1.727 0.961 1.566 1.2.800 5.061 2.841 1.671 1.700 0.962 1.607 1.2.903 5.102 2.830 1.607 1.671 0.963 1.625 1.3.000 5.180 2.818 1.701 1.657 0.963 1.647 1.647 0.965 1.647 1.3.300 5.187 2.807 1.720 1.631 0.966 1.668 1.3.300 5.209 2.755 1.726 1.619 0.966 1.668 1.3.300 5.243 2.784 1.732 1.607 0.967 1.675 1.3.300 5.243 2.773 1.731 1.602 0.967 1.675 1.3.300 5.243 2.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.731 1.602 0.967 1.675 1.3.300 5.243 5.773 1.773 1.774 1.675 1.473 5.774 1.675 1.473 5.774 1.474 1.475 1.474	000	4	1004	300°1 40°0 30°0 30°0 30°0 30°0 30°0 30°0 30°0	
2.800 5.001 2.841 1.671 1.700 0.962 1.607 1. 2.903 5.102 2.830 1.697 1.677 0.963 1.625 1. 3.000 5.140 2.818 1.701 1.657 0.964 1.641 1. 2.100 5.158 2.818 1.711 1.647 0.965 1.651 1. 3.200 5.187 2.807 1.720 1.631 0.966 1.662 1. 3.200 5.212 2.745 1.726 1.619 0.967 1.653 1. 3.600 5.212 2.784 1.732 1.607 0.967 1.615 1.	2.800 5.001 2.841 1.671 1.700 0.962 1.607 1.2903 5.002 2.830 1.687 1.677 0.963 1.625 1.625 1.000 5.100 2.816 1.701 1.647 0.964 1.641 1.647 0.964 1.641 1.300 5.187 2.807 1.720 1.631 0.966 1.662 1.300 5.209 2.795 1.726 1.619 0.966 1.662 1.300 5.243 2.784 1.732 1.607 0.967 1.675 1.300 5.243 2.773 1.731 1.602 0.967 1.675 1.300 5.243 2.773 1.731 1.602 0.967 1.675 1.300 5.243 5.773 1.731 1.602 0.967 1.675 1.300 5.243 5.773 1.731 1.602 0.967 1.675 1.300 5.243 5.773 1.731 1.602 0.967 1.675 1.300 5.243 5.773 1.731 1.602 0.967 1.675 1.300 5.243 5.773 1.731 1.602 0.967 1.675 1.400	0.00	• -	-	7-3 N40-0 015	
2.903 5.102 2.836 1.697 1.617 0.963 1.625 1.300 5.160 2.818 1.701 1.657 0.964 1.641 1.300 5.158 2.818 1.711 1.647 0.965 1.651 1.551 1.300 5.187 2.807 1.720 1.631 0.966 1.662 1.300 5.230 2.745 1.726 1.619 0.966 1.668 1.300 5.232 2.784 1.732 1.607 0.967 1.615 1.615	2.903 5.102 2.636 1.697 1.677 6.963 1.625 1.300 5.140 2.618 1.701 1.657 0.964 1.641 1.651 0.965 1.651 1.651 0.965 1.651 1.651 0.965 1.651 1.300 5.167 2.967 1.723 1.631 0.966 1.662 1.300 5.209 2.755 1.726 1.619 0.966 1.668 1.300 5.20 2.785 1.732 1.607 0.967 1.675 1.300 5.20 5.785 1.731 1.602 0.967 1.675 1.		• -	2001		
3.000 5.140 2.818 1.701 1.657 0.964 1.641 1. 3.100 5.158 2.818 1.711 1.647 0.965 1.651 1. 3.200 5.187 2.807 1.720 1.631 0.965 1.662 1. 3.300 5.209 2.755 1.726 1.619 0.966 1.668 1. 3.400 5.232 2.784 1.732 1.607 0.967 1.615 1.	3.000 5.140 2.818 1.701 1.657 0.964 1.641 1. 2.100 5.158 2.818 1.711 1.647 0.965 1.651 1. 3.200 5.187 2.867 1.720 1.631 0.966 1.662 1. 3.300 5.209 2.755 1.726 1.619 0.966 1.668 1. 3.400 5.212 2.784 1.732 1.607 0.967 1.615 1.	, ,		775		
3.000 3.190 2.218 1.711 1.647 0.965 1.651 1. 3.200 5.187 2.867 1.723 1.631 0.966 1.668 1. 3.300 5.209 2.795 1.726 1.619 0.966 1.668 1. 3.400 5.212 2.784 1.732 1.607 0.967 1.615 1.	3.000 3.190 2.110 2.110 1.001 1.001 0.905 1.001 3.200 5.187 2.007 1.720 1.631 0.906 1.662 1.002 1.300 5.209 2.795 1.726 1.619 0.906 1.608 1.008 3.400 5.212 2.784 1.732 1.607 0.907 1.615 1.300 5.243 2.773 1.731 1.602 0.907 1.615 1.000	,	٠.	> 6 F = 1	265 T EST - 2	265-1 865-13 613-1
3.200 5.187 2.867 1.720 1.631 0.966 1.668 1. 3.300 5.209 2.765 1.726 1.619 0.966 1.668 1. 3.300 5.212 2.784 1.732 1.607 0.967 1.615 1.	3.200 5.187 2.807 1.720 1.631 C.966 1.662 1.303 5.209 5.279 2.795 1.726 1.619 C.966 1.668 1.30.400 5.272 2.784 1.732 1.607 0.967 1.675 1.30.400 5.243 2.773 1.731 1.602 0.967 1.675 1.400		-	6.5.	53 C. 455 C. 455	5.5°1 656.0 652.1 010.0
3.200 5.187 2.867 1.720 1.631 0.966 1.666 1.300 3.209 2.795 1.726 1.619 0.966 1.668 1.300 3.209 2.784 1.773 1.607 0.967 1.615 1.860 0.967 1.615 1.	3.200 5.187 2.867 1.720 1.631 0.966 1.666 1.300 5.209 2.755 1.726 1.619 0.966 1.668 1.3.400 5.212 2.784 1.732 1.607 0.967 1.615 1.3.500 5.243 2.773 1.731 1.602 0.967 1.615 1.	.,		1.529	53 0.954 1.928	2.(12 1.753 0.959 1.928
3.303 5.209 2.755 1.726 1.619 0.966 1.668 1. 3.400 5.212 2.784 1.732 1.607 0.967 1.615 1. 3.600 4.24. 2.77 1.731 1.602 0.967 1.613 1.	3.500 5.209 2.755 1.726 1.619 0.966 1.668 1.3.60 3.400 5.232 2.784 1.732 1.607 0.967 1.675 1.3.500 5.243 2.773 1.731 1.602 0.967 1.675 1.		_	B.5.1	53 0.959 1.528	855.1 0.050 0.050 1.628
3.400 5.232 2.784 1.732 1.607 0.967 1.675 1.	3.400 5.212 2.784 1.732 1.607 0.967 1.675 1.	~	-	1.014	515*1 *55* 24	515-1 +55- 004-1 100
1 3 Enc. 4 24 2,173 1,731 1,602 0,967 1,615 1,	3.500 5.243 2.773 1.731 1.602 0.967 1.675 1.		_	63 1.508	800.4 600.4	800 T C97 T T T T T T T T T T T T T T T T T T T
2.201 10.00 30.00 10.00 20.00 20.00 1		_		7500		

TABLE 6 15 DEGREE SHOCK WAVE GENERATOR

-	S LEGREE	SHGCK	DAVE GENE	RATCR.	X = 70.0	1 0			S DEGREE	SPECK	MAVE GENE	GENERATOR.	x = 75.0	¥ 0	
:	1					_		Y CH	I	_		1 /		RHC	/ 11
(F)	•	, <u>,</u>	APC 14F	1 [NF	181 ⊃	KHCU INF	TT INF	•		P INF	RHC INF	- INF	U. D	_	Ż
	ć	¥ 4 7	•.		3000	Ü	0.432	000.0	000.0	2.000	C-452	4.426	00000	0.030	0.432
) .) (, , ,) (1		0.053		0.778	0.00	2.030	7.000	6.463	4.320	0.615	C . Z . Z) (
4 C	7000	2.455		3.536	0.735	٠	5.835	0.675	2.5e1	2.000	1 7 6 0	3.7.6	01/0	0.500	9.00
· ()	2 P 74	. 45.5	_,		L. 764	ر.	C - 864	0.10	2.136	2.000	1.364		27.7	44	88.0
1 2 6	2.530	2.435	.,		0.785	_	0.884	3.125	2.931	2.000	71.00	0 m 3 d m	7 7 9 0	4 G	808 C
· · · · · · · · · · · · · · · · · · ·	655.2	2.455	• ,		0.795	_	C.848	C-15C	2.910	707.2		- 4	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.440	3,906
	£.0.5	6.44.5			C-804		9.0	6.175	155.2	0000		, , ,		0.462	0.915
·)	-11-:	2:455	,		(B)		516.0	0.200	3.064	000	1000	16.1	4 CC	0.525	0.526
	. 1	554.7			0.829		0.927		9.1.c	2000	* C = C	3.016	0 0 0 1 0 1 0 1 0	2.561	0.938
ń,	*	2.45.5	,,,		5.842	_	0.938	008.0	0 4 4 4 C	000	700.0	50.0	0.856	0.585	0.947
	204.5	3.44.5			C. 854	_	9 7 6		2 4 3 1) a c	1000	7 . 34.8	0.866	0.664	0.953
•	. 4 F.	344.7	•		C.853	.,	> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		3 6 1 2		0.721	2.758	C. 876	0.631	0.96°
	3.66	7.44.4			· · · · · · · · · · · · · · · · · · ·	•) (* u	3,00	1.577	0.736	2.680	6.883	0.652	996.0
	, e				8 8 8 C	•	0,00		0.00	1.577	6.766	2.582	C. 895	ે. ૯85	0.972
		7.7.2	•		: . : . : . : .		0.077		9.75	1.966	0.785	2.503	408.0	0.710	386°0
(O)	. 613				2 7 C		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	000 C	4.0.4	1.566		2.425	0.911	0.739	0.985
; ;	€ 1 D	7. 104		7			7 00		40.1	1.555	0.88.0	456.5	615.0	C.762	0.989
****	3.5.5	, 5,	_	2	1 7 C			100	- C	1.555	∠*a*○	2.321	6.552	C.177	C+7.40
ر •	, , , , , , , , , , , , , , , , , , ,			30.4.	6		7 70 0	301-7	4.202	1.955	0.855	2.005	6.526	0.142	376.0
, , , , , , , , , , , , , , , , , , ,	() () () () () () () () () () () () () (*						1.200	147.4	1.543	1.48.0	2.251	6 75 7	C. BCC	156.0
	71.	•					0.497	1.300	4-284	1.943	C.873	2.22€	C. 932	ر ا ا	J (
		- C	_		\ \(\frac{1}{2}\)		C. 34.R	004.1	4.316	1.541	€88.0	2.262	0.034	C.824	ナ ナ ナ ・ ・
) F 4		· ·		٠.			0.000	1.533	4.355	1-532	⊖ 8 • ⊖	2.172	565	N	
) (•		191°	. 65.	9.00 E	¥85.0	1.600	4.35.7	1.532	\$0 5 .0	561.7	- 12 · 13 · 1	* B * C	
000	· ()	90		•	547.3		000.1	1.700	4.4.8	25.5	116.0	75000	rer: 0	100.0	
) 7	260	110		T.	0.440		200.1	008-1	234.4	725-1	625.0	*10.2	1 40	4 di 40	1.030
700	* , , ,	¥1.		3	* * * * * * * * * * * * * * * * * * * *		000.1) () ()			0.53	010	0.40.0	006.0	1.000
0000	115.4	(), • ;		1.3	\$?				1.0.1	7 0	7 () () () () () () () () () (1.471	0.947	216.0	1.000
; ;	7.40.1	75		ູ່	* 1 2 • (000	0000.6	4.671	a 5 a . I	0.578	1.940	545*3	C.528	1.060
; ;		, , , ,		、 1	• • • • • • • • • • • • • • • • • • •		2021	201.	12705	1.666	664.5	# C. 8	135-7	346.0	1.000
•				C 4	3,50		300.1	004.5	4.7.4	1.875	100.1	1.872	0.552	4.0	1.000
* ·	- 4			-	365		1.000	2.500	213.4	1.864	1.011	1.844	5 C C C C C C C C C C C C C C C C C C C	775	्र १ १
· ·		1		~	T		1.000	204.2	4.803	7.887	0.0 · 1	1.758	6.00	r	000
, • , .				· .7	(40.0		1.000		4.966	1.44.	1.043	1.754	7.65) (
,		7 6		_	195		1.000	2. ACC	5.cc	1.630	1.057	17.	20.0	(1) • 1) () (
•	, ,			T	4000		1.000	735.2	5.010	1.418	<u>ر</u> .		ε . • · · ·	7 7 7	
•				1.000	167.0		1.000	700°+	5.113	1.613	960°	1.4.1	\$ 0 5 0 5 0	1	2000
• -				4	,05.7		1.036	3.160	2,1.3	τ. μ. ι	_	27	ر . د رون د رون	000	•
				r.	3.325		1.000	3.200	#01.	I (7 (3 h) :) :
•				77.1	1.5.		1 - 000°	30€-€	5.230	्र इ.स		Ε . Ο μ	- C - C - C - C - C - C - C - C - C - C		
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	:		1.00	760.		1.000	3.400	5 4 5 ° °	B	1.1.	· * * * * * * * * * * * * * * * * * * *	2 4 4 5 C	7711	000
(0)	* · ·	7		1.576	-	1.389	1.000	ગ0ુઙ•⊾	192.5	L	7 3 1	. 0	•		,) •

TABLE 6 — CONCLUDED

	11 (1608)	FSECCE	MANE GENE	UENEF ATON,	X = 85.	100			5 CEGREE	SPCCK	MAVE GENE	GENERATUR,	X = 95.(# C O	
103 x		, , , , , , , , , , , , , , , , , , ,	PHC / BHE PHE	1 / T) o	RHCU / RHJU INF	17 / 17 INF	YCCHI) a 1 v	RHC / RHU INF	1 / 1 INF	0 0 N	RHCU / RHCU INF	11 / 11 IN
30000	0.000	1.375	11.00	4.426	ૅ	222*2	4	000.0	~	.13		7	0.0	9	0.432
3 + CO * C		1.274	000	•	.56x	C-182	~ r	0.0.0	1.785	1.136	C.263	4.232	0.535	0.144	0.676
		1.375	126.7	0 40	0		3 -) (C	- `	-	•	2	20	.	0.744
\$ 77		1.375	C • 3 0 3	۰ ٥	~		œ	221.5				2 ~	2 =	, ,	0.874
2.153		1.375	() 4 • ()	3	~		8	0.150				3	~~		0.844
3-175		1.175	904.0	3.384	~		8	176	•	.13		2	75	5	0.858
766.7		1.375	6.413	1.329	7		8,	0.5.0	٠.	13		*	2	• 24	C. 868
) \$ / • · ·		1.37	574.3	3.204	~		99	C.25C	٠.	. 12		39	38	52.	0.883
		7.6.	~ \$ 4 • 7	3-112	.		<u>ه</u> .	0.300	٠.	• 12	,	5.	5	.21	0.894
ć;;		4.6.1	ლი წ • • • • • • • • • • • • • • • • • • •	E 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	انت		6	0.35c	7	=		91.	8	• 28	406.0
 • .		4 .) • • • • • • • • • • • • • • • • • • •	6 2 9 2 3	e d		5 6	04.0		. 1 C		Ž.	2	57.	216.0
		0	→ c × · · ·	1 E D 1 7	80		3	0.44.0		()		ξ.	۲) وا	. 31	716.0
, , ,		4000	T 0	Z 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.		5	0.500	٠.	တ် (•	9	4 0	÷ 32	0.926
		* 05	,	7 - C - C	5		* 6	200.0	•	٥٠	•	-	9	46.	0.938
) (a		* 36 * 1	# 7 	000.7	E C		5 6	0.700	- '	•	٠.	3	-	36	546.0
		706.1	r * • • •	00000	,		?	0	•	ۍ د د	•	ζ,	80 1	E	756.0
		***	7000		6		,) ()) ()) .	•	•	•	÷ .	Dr. (, w	0.966
;		304	1 'C'	925	,		, c	330 -1	٠,	٠ د د	•	4	<u>.</u>	7	0.972
		7 4 7	P 4 3 4	7 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- 6		5	201-1	•	, c	•	2 5	7 :	•	7.5.0
		7 20 4	7 7				- 0	105.1		٠ ر			. ·		, e
		\$ J 1	1000	7.207	•		9 0	7 (4)	٠,	, (_ 1	9 -	,,	, v	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
· · · · ·		1 . 36 4	N. 4. U	2.176	. ;		2 0	700	2 ~	ر ان ر			7 .	. 4	7 0 0 0 0 C
			. 6	2.134	Š		6				` "			7	16700
77.		1.364	C. e. 5 3	2.089	ő		9	1.730	٠.	•		0	, ~		46.00
() 6.1		1.364	6.663	2.055	5		9	008-1	4			3	۳,	4	966.0
2. • • • • • • • • • • • • • • • • • • •		1.364		2.026	ž.		6	1.433	3,	-	4.	2	7	4.0	0.994
, 60°		1 - 30 4	C. f.36	1.988	4		6	700.7		-	۷.	S	0.544	50	556.0
ं : • :		1.364	\$ 0 0 0	1.962	, ,		6	2.100	٥	• Ĉê	S.	6	4	15	556.0
		1 . 16 4	0 - F	166.	\$ U		5		•	3	٠, ٠	, i	*	5.	000.
)		4000	2				0	2000	ų r	L	ຼີ່	7.0	1 4	3	
, (C) 3		1 - 36 +	C - 7 3 3	1.950	ું		0		. ~) (. •		7.0.0		7.00
		6 .	194.0	1.916	5.5		S	2.00.			٠.	ac.	, 1	, ,	
		1. 16.	C - 763	1.783	4.		5	2.10.	بد		41	8		. 2	000.1
() (1) (1) (1) (1) (1) (1) (1) (1) (1) (1.364	6.173	1.765	5.		0	3.904	ar.	. C 4	~	1.808	3	υ, υ,	1.000
, , ,		1.304	0.793	4	5		0	700	3	47.	ď.	1.752	¢ 5	.56	1.000
· .		1.364	6-793	7	\$		Ö	3.00.6	J.	٠,۲	٠.	1.764	. 55	۶.	000-1
-		1.364	~ ·	Ş	ç		$^{\circ}$	3.100	٠.	, C4	ς.	1.744	95.	7.	1.000
7		1.36.	514.5	Ç ,			1.000	3.200	Ċ	1.640	40	1.729	3.96.0	5.7	1.03:
		4		\$	9		်	30c	۰	~ J•	9	1.702	÷.	3.	1.00
, , ,		1.32	6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1.655			ر. د	3.400	ب	.03	9	1.683	7	4	1.090
		σ • • • • • • • • • • • • • • • • • • •	() () ()	5	Š		ල ට	3.500	5.1.3	. C3	•	1.664	÷	9	1.000
							•								

TABLE 7

7.5 DEGREE SHOCK WAVE GENERATOR

15 DEGREE SHOCK WAVE GENERATOR

TABLE

, r	0.254	0.266	0.271	0.412	0.158	0.245	0.182	0.157	0,151	0.138	0.130	, c	0,160	0.160	0.149	146	6.171	0.178	
*:	7360	0.360	7570	ं <mark>ी</mark> भे	1.340	0.544	0.417	796.0	747°	F36.	0.174	c c	0.207	0.203	161.0	0.41.0	455.	3 . 3 a.c.	
ø	400.0	0.104	0.173	800°0	0.020	0.104	0.126	0.098	0.101	0 a C • C	0.0 x 3	300°C	901.0	C.101	0.00a	δ0.0°0	0.106	0.117	
* Q	1.323	10274	1.337	2.250	5.034	C # Q 5 3	0.304	5.438	, 76,	7 4 4 R.F.	2677	044.0	147.	P. 925	[C8.0]	0.961	1.020	0.010	
S	े 1 े	2.10	2 B C	7.8F	2.20	0.40	्ट• :	ر د • ،	1.45	, y.	(, C, •	0.44.0	0.40	£0.€	, ,	3.25	74.4	ی تان ۲	
N, CIII	0.0	75.5	C e c.	٠ ٠	0.65	יא א	c • α τ	U • C †	y . 7	(* y *)	C .	C,	٠,٠)	, , ,	5 U.C	ं ,	C • 3 0	C • u C	
θ_1	28 6 0	F. 26.	0.359	2.253		5.212	3.17E	0.170	0.166	₩	- 10.2 - 10.2	7.16.7	6.162	. 41.	2.165	रव!•	.230		25.50
* -	0.446	447.0	5.442	ब इ •	6.54.5	1 7 7 . ()	. 116	r d c	7220		*, *, *.	121	356.	ان د د	166.	640.	13.0	V	•
Э	3.136	F C	0.1.0						7 C •	ā	£ 0.		-	C. 7.	च ल € • (30	, , , , , , , , , , , , , , , , , , ,	• •
*		•	() () () () () () () () () ()	•	•	. ,,			•	•	:	•		- u-					•
	4	´•	· ·		٠,			٠.	-	7.	ĭ.			0.00		;	1		
	•	•			,	٠.			•	•		•	•		-				

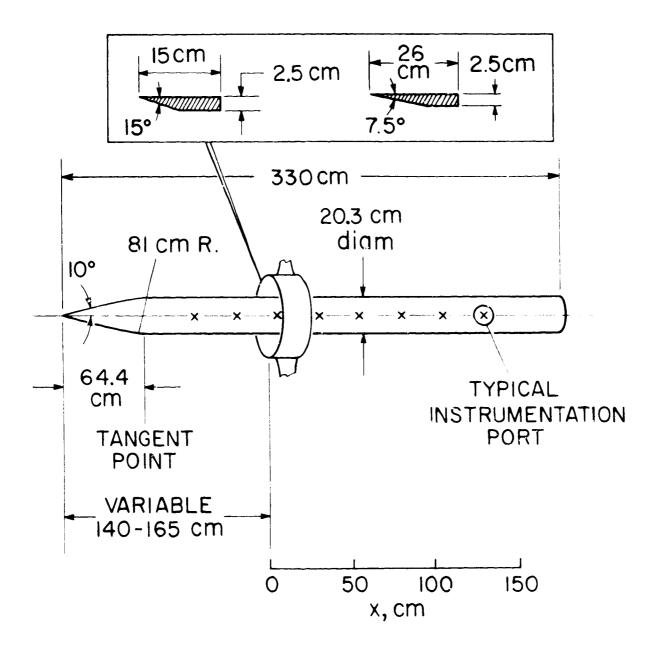


Figure 1. - Test model.

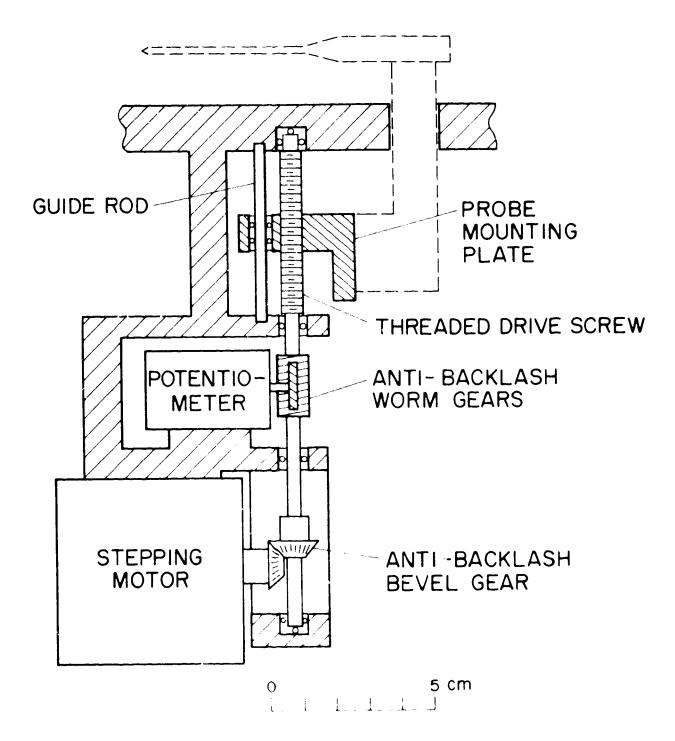


Figure 2. - Survey mechanism.

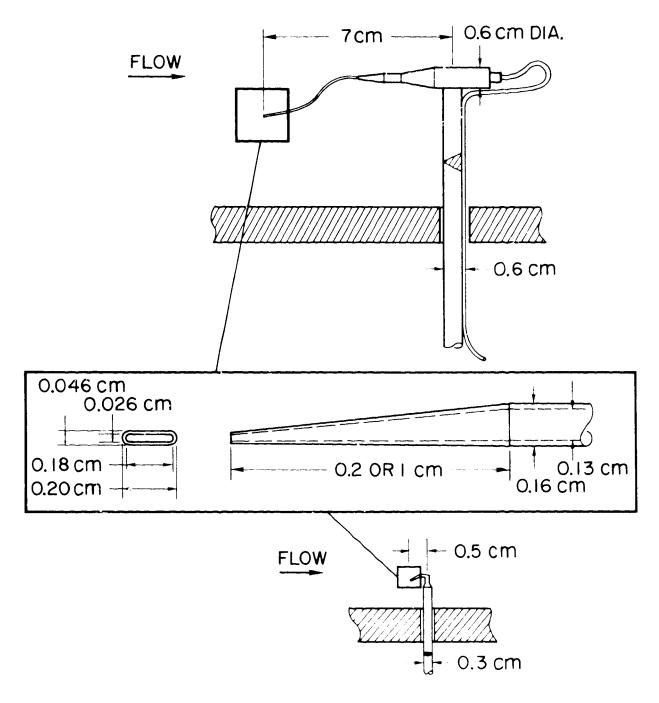
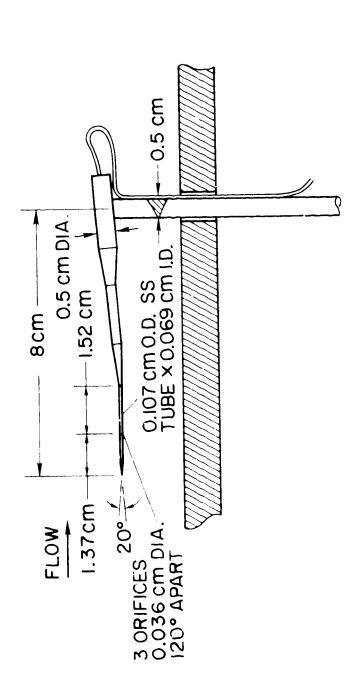


Figure 3.— Pitot pressure probes.



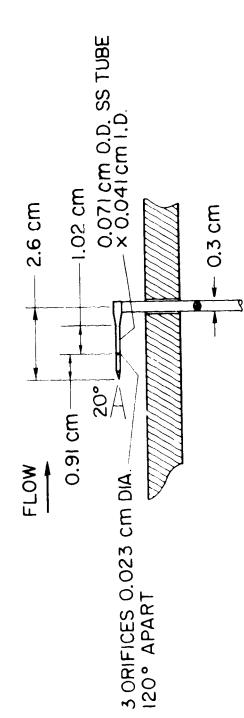


Figure 4.- Static pressure probes.

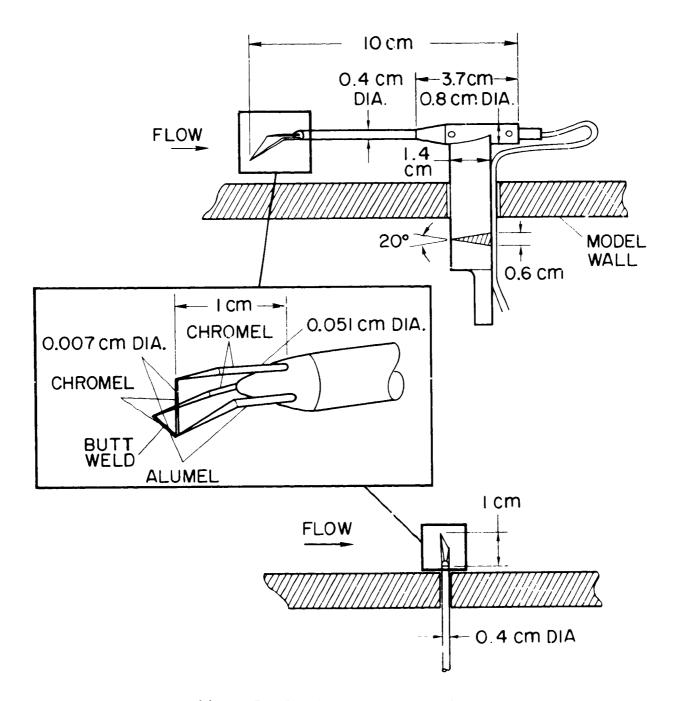


Figure 5.- Total temperature probes.

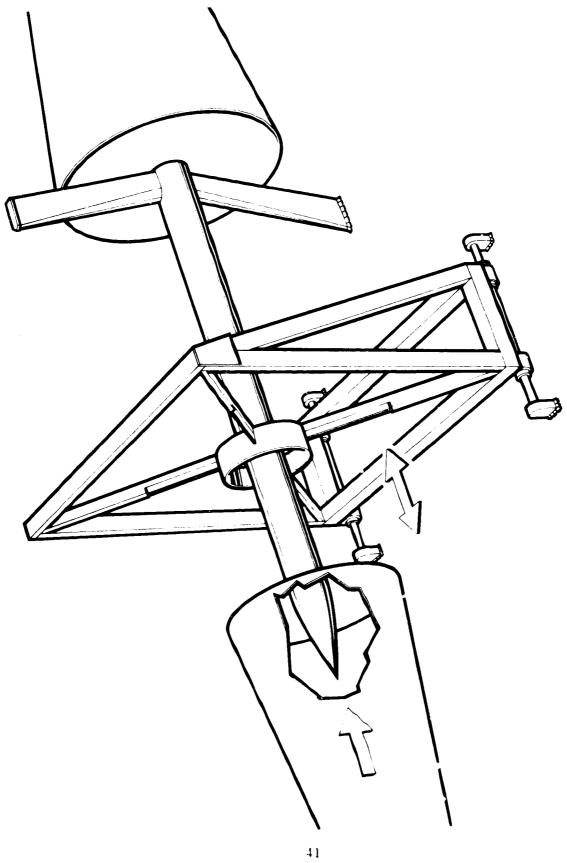


Figure 6.- Shock-wave generator traverse mechanism.

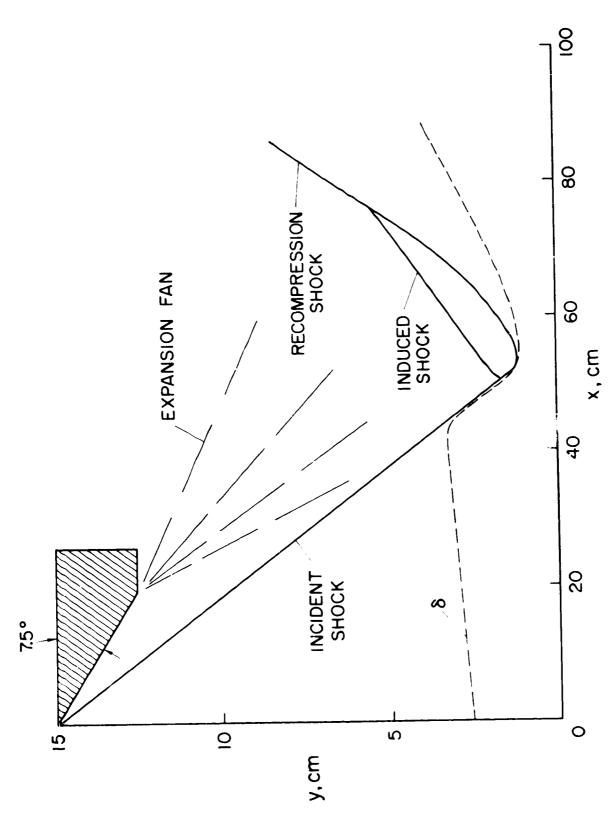
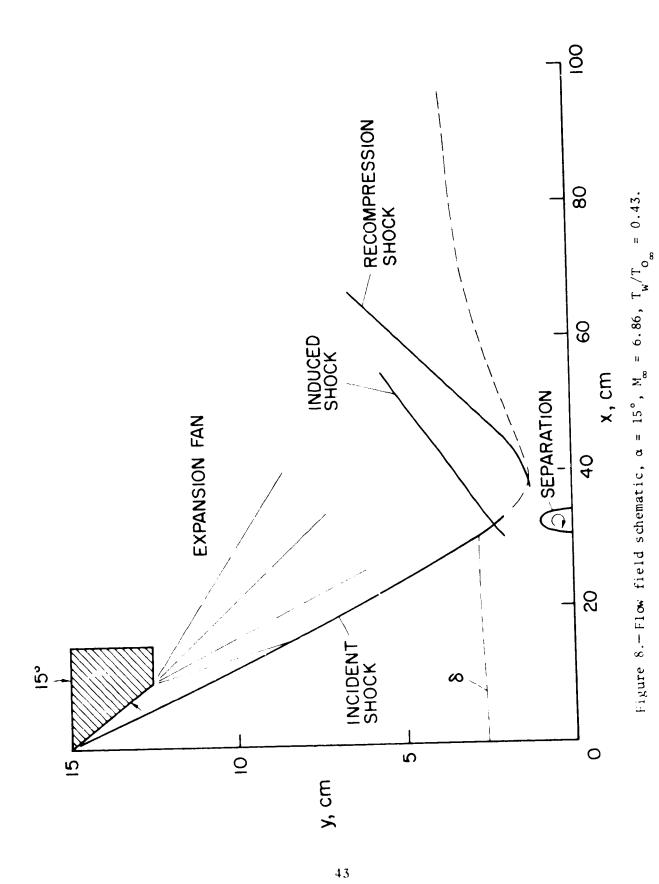


Figure 7.- Flow field schematic, $\alpha = 7.5^{\circ}$, $M_{\infty} = 6.86$, $T_{W}/T_{0_{\infty}} = 0.43$.



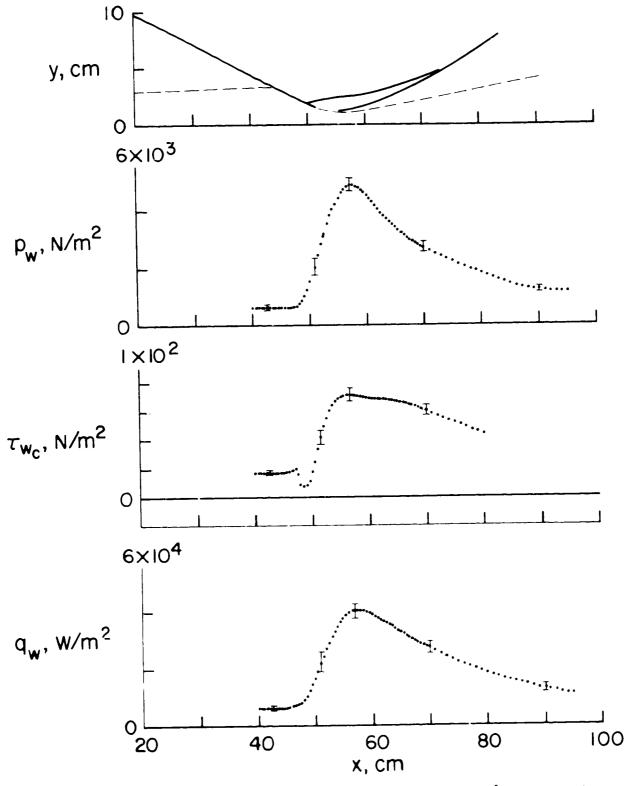


Figure 9.-Measurements along the model surface, α = 7.5°, $M_{\rm w}$ = 6.71, $T_{\rm w}/T_{\rm o_{\infty}}$ = 0.43.

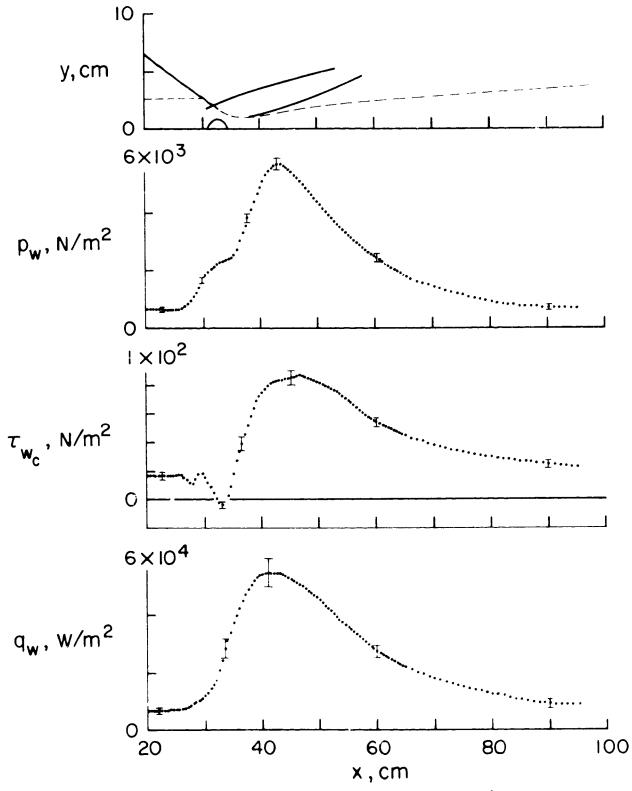
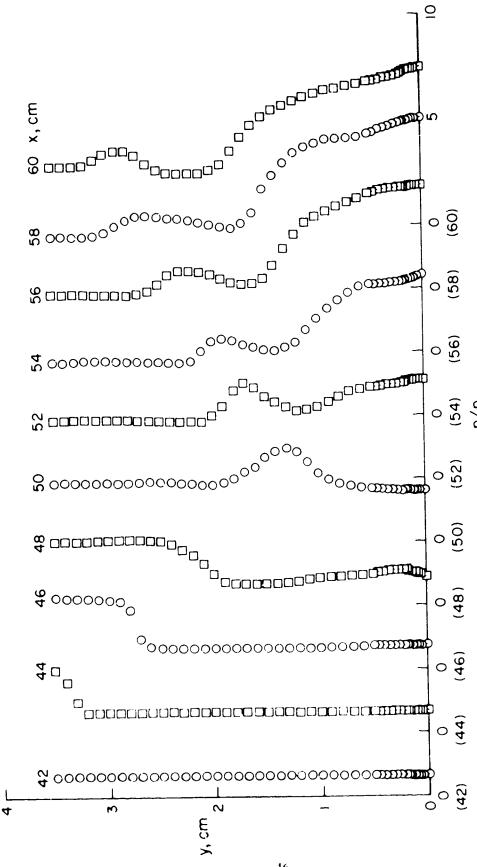
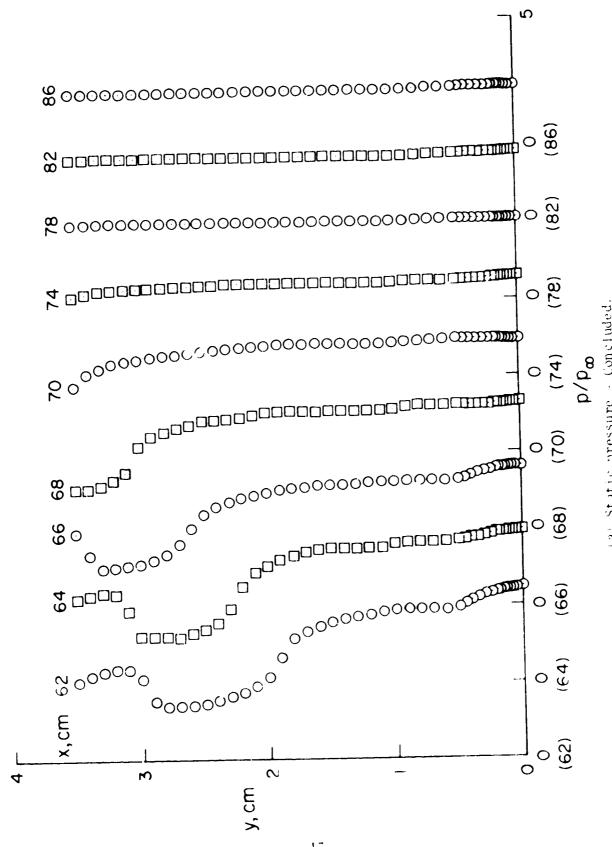


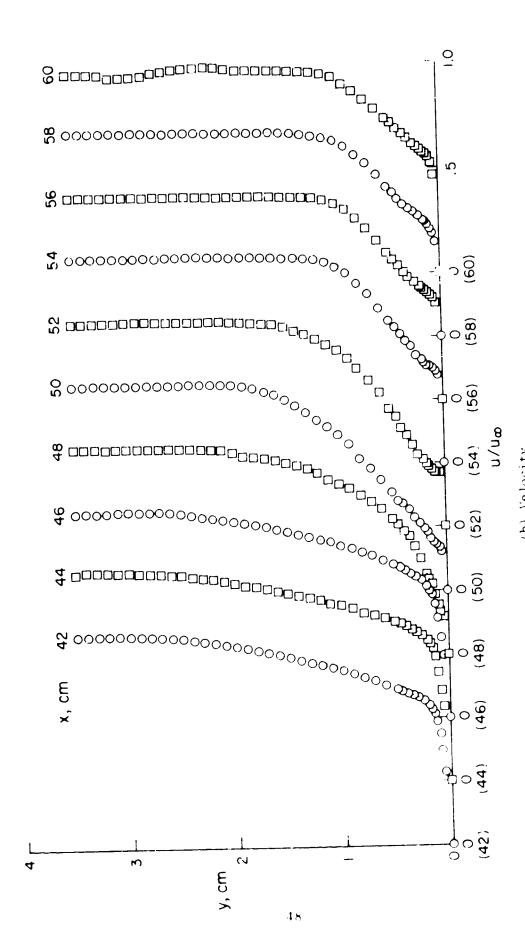
Figure 10.— Measurements along the model surface, α = 15°, M_p = 6.86, $\Gamma_w/\Gamma_{o_{\infty}}$ = 0.43.



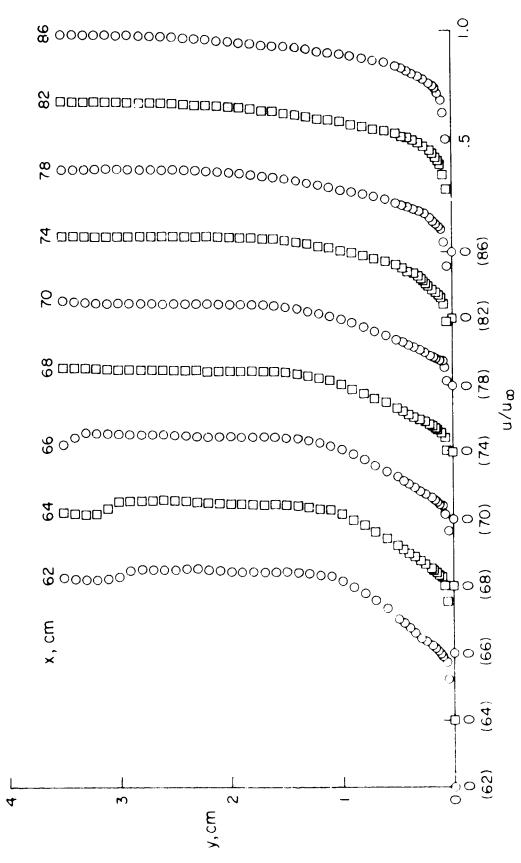
(a) Static pressure. Figure 11.- Flow field profiles, α = 7.5°, M_{∞} = 6.71, T_{ω}/T_{\odot} = 0.43.



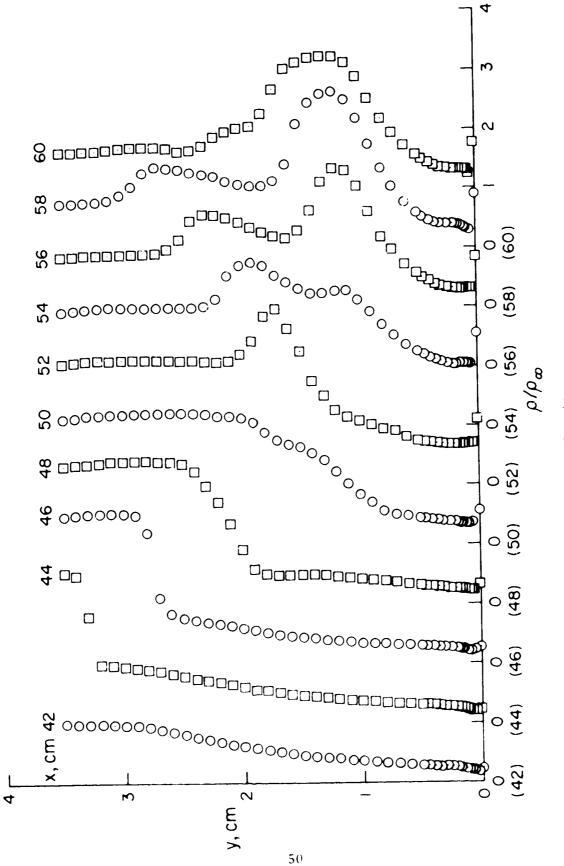
statte pressure concre

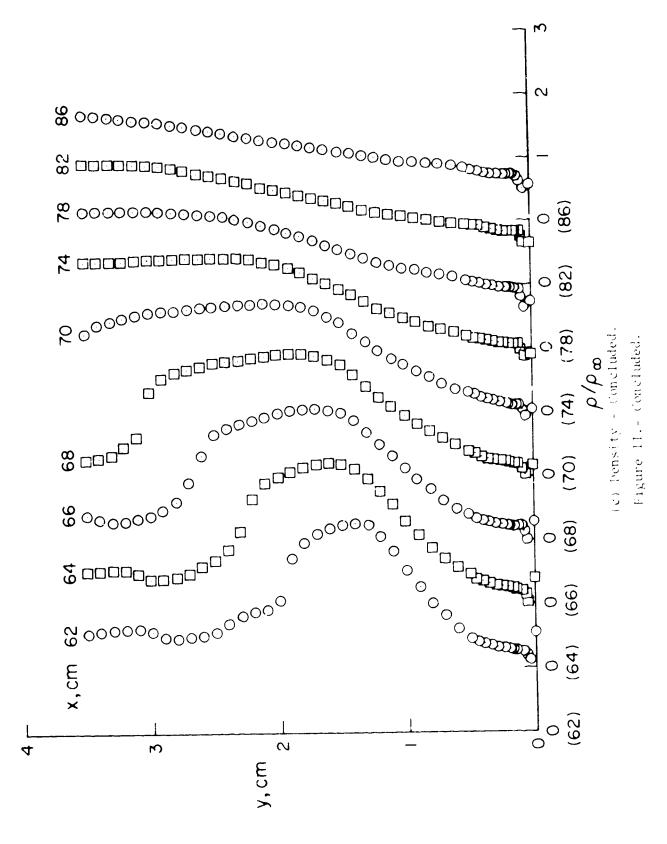


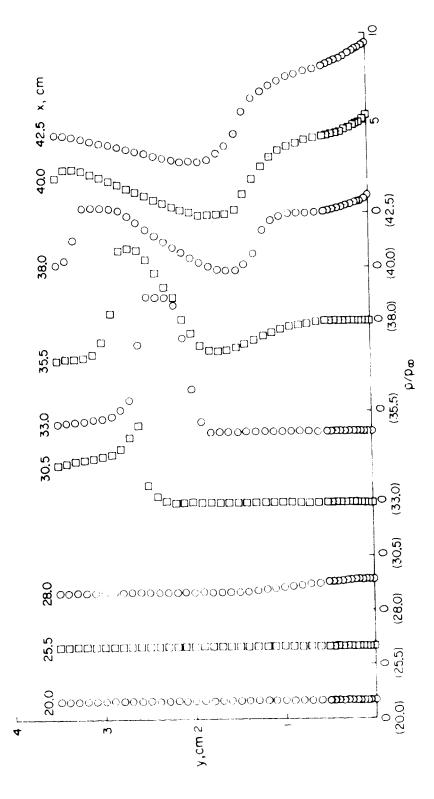
ionre 11.- Continued.



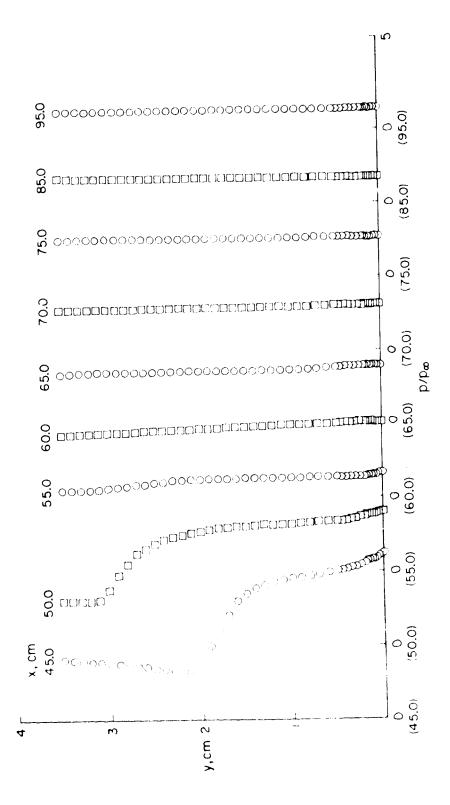
(b) Velocity - Concluded. Figure 11. Continued.



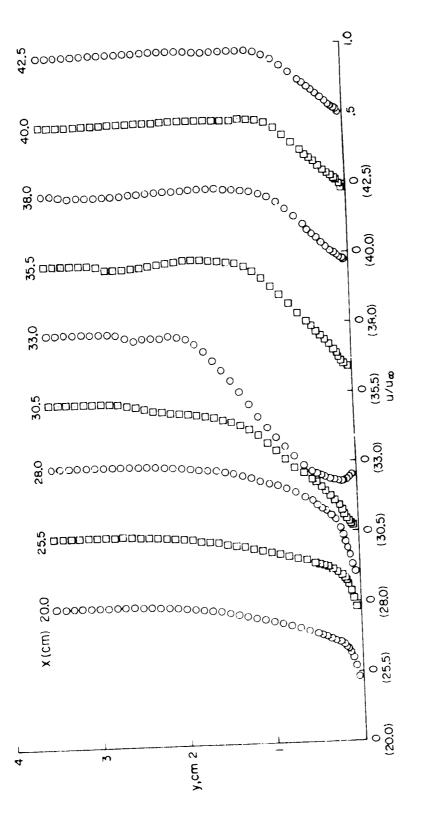




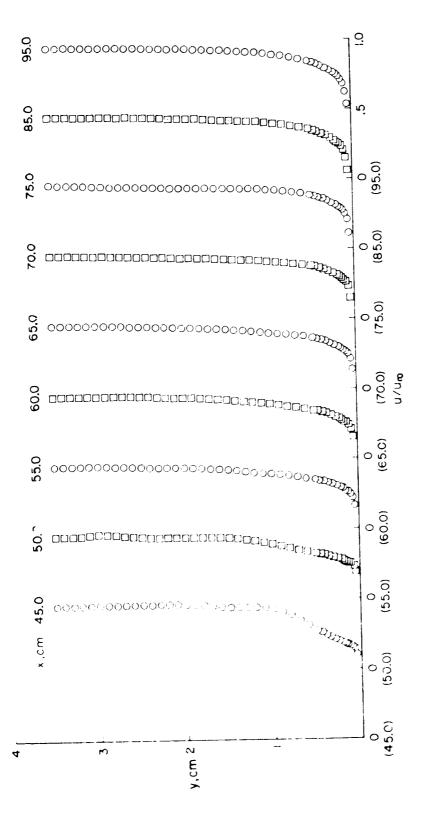
(a) Static pressure. Figure 12.- Flow field profiles, x = 15°, M_{∞} = 6.86, T_{w}/T_{\odot} = 0.43.



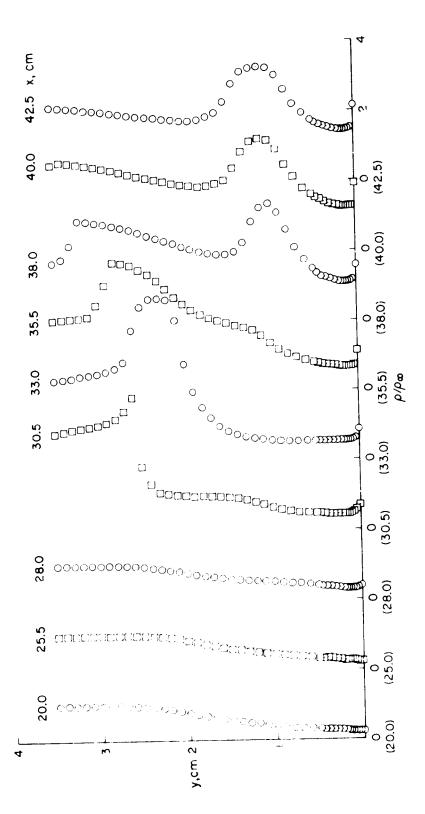
(a) Static pressure - Concluded.Figure 12.- Continued.



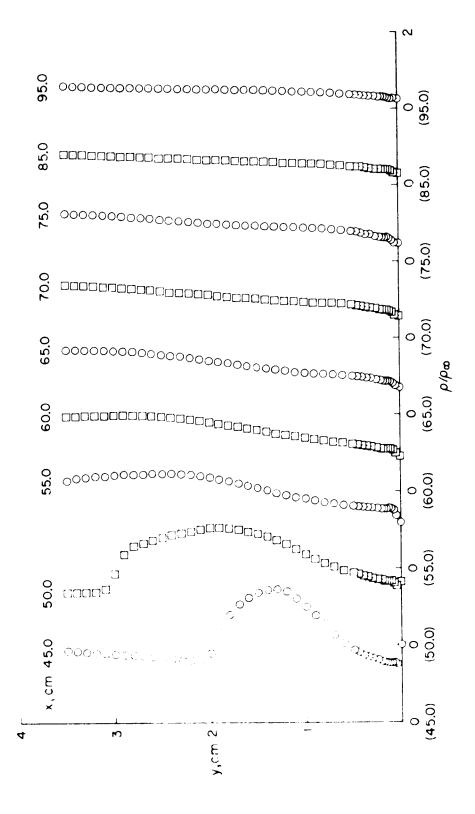
(b) Velocity.
Figure 12.- Continued.



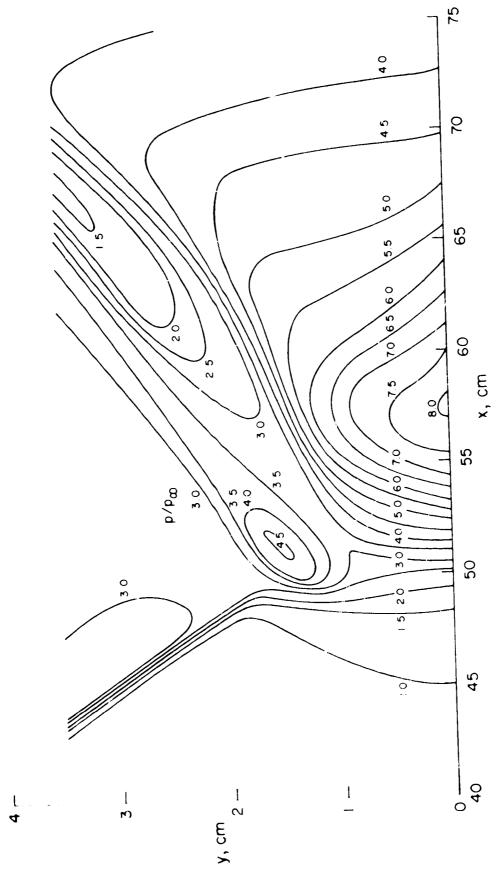
(b) Velocity - Concluded.
Figure 12.- Continued.



(c) Density. Figure 12.- Continued.



(c) Density - Concluded. Figure 12. Concluded.



(a) Static pressure. Figure 13.- Flow field contours, α = 7.5°, M_{∞} = 6.71, $T_{\rm w}/T_{\rm o}$ = 0.43.

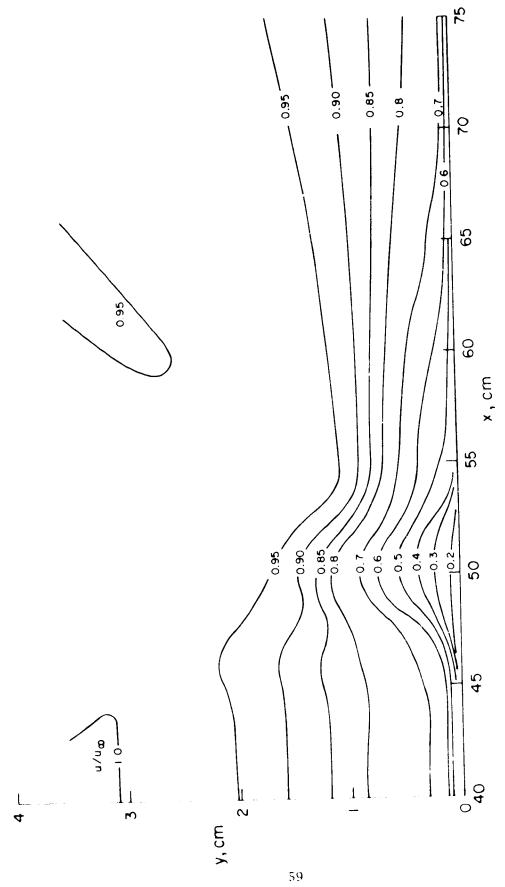
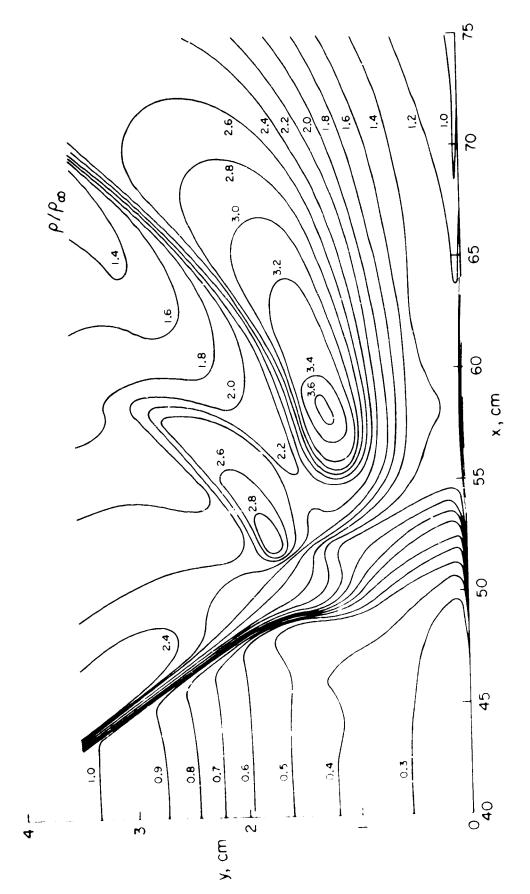


Figure 13.- Continued. (b) Velocity.



(c) Density. Figure 13.- Concluded.

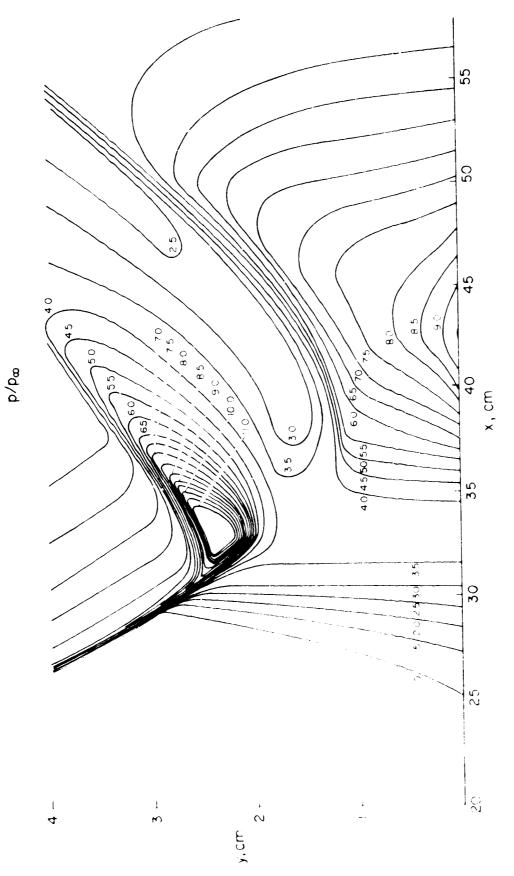
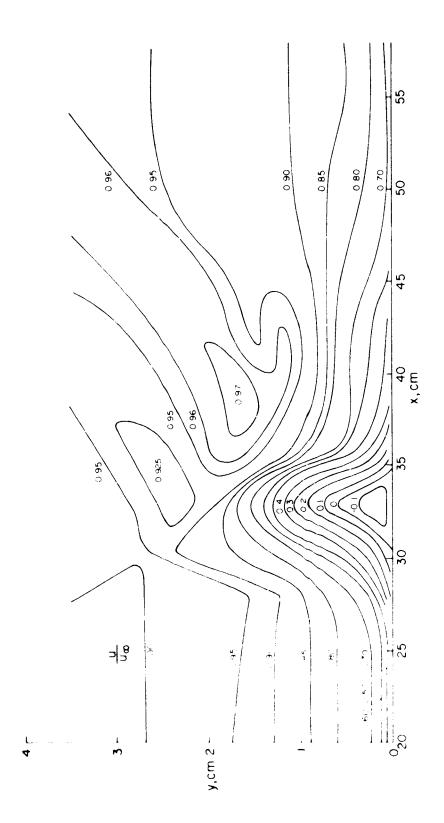


Figure 14.- Flow field contours, $x = 15^{\circ}$, $M_{\infty} = 6.86$, $T_{\omega}/T_{\omega_{\infty}}$ 0.43.

(a) Static pressure.



(b) Velocity.Figure 14.- Continued.

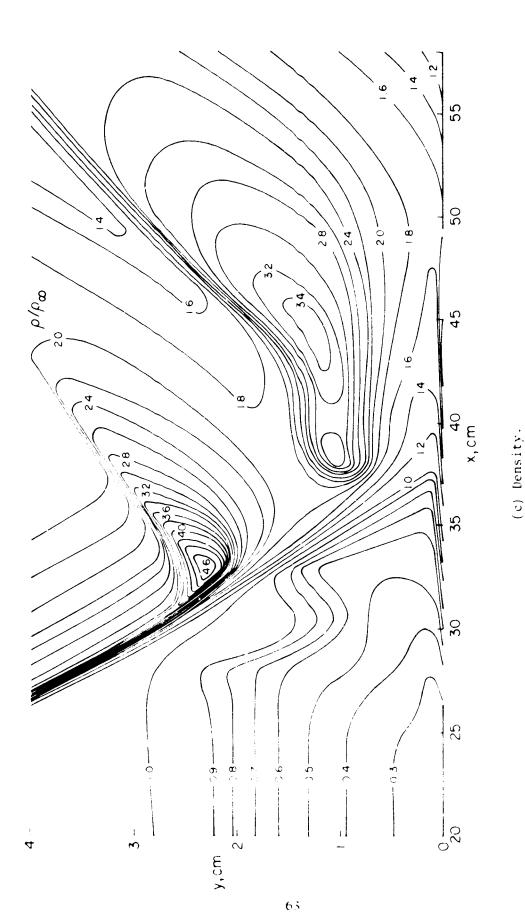


Figure 15.- Streamline contours, α = 7.5°, M_{∞} = 6.71, T_{W}/T_{0} = 0.43.

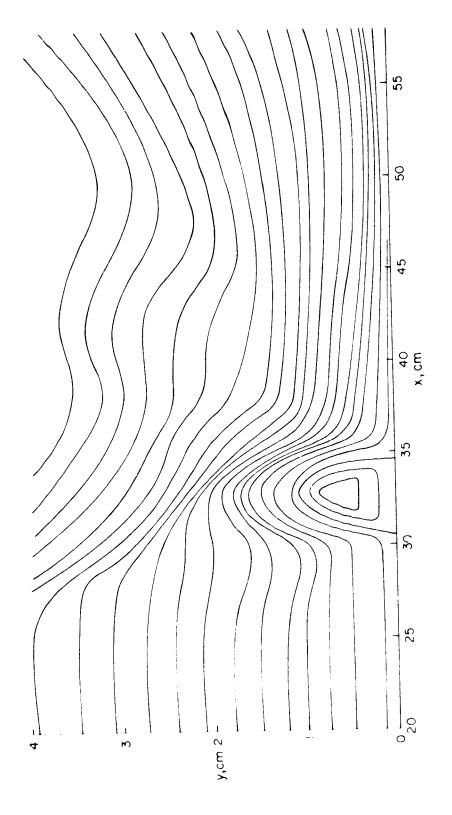


Figure 16.- Streamline contours, $\alpha = 15^\circ$, $M_\infty = 6.86$, $T_W/T_0 = 0.43$.

END

DATE

JUN 13 1975